

Durability and physical characterization of anti-fogging solution for 3D-printed clear masks and face shields

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Background. The COVID-19 pandemic brought forth the crucial roles of personal protective equipment (PPE) such as face masks and shields. Additive manufacturing with 3D printing enabled customization and generation of transparent PPEs. However, these devices were prone to condensation from normal breathing. This study was motivated to seek a safe, non-toxic, and durable anti-fogging solution. **Methods.** We used additive 3D printing to generate the testing apparatus for contact angle, sliding angle, and surface contact testing. We examined several formulations of carnauba wax to beeswax in different solvents and spray-coated them on PETG transparent sheets for testing contact and sliding angle, and transmittance. Further, the integrity of this surface following several disinfection methods such as soap, Isopropyl Alcohol, or water alone with gauze, paper towels, and microfiber, along with disinfectant wipes, was assessed. **Results.** The results indicate a 1 : 2 ratio of carnauba to beeswax in Acetone optimally generated a highly hydrophobic surface (contact angle $150.3 \pm 2.1^\circ$ and sliding angle $13.7 \pm 2.1^\circ$) with maximal transmittance. The use of soap for disinfection resulted in the complete removal of the anti-fogging coating, while Isopropyl Alcohol and gauze optimally maintained the integrity of the coated surface. Finally, the contact surface testing apparatus generated a light touch (5000 N/m^2) that demonstrated good integrity of the antifogging surface. **Conclusions:** This study demonstrates that a simple natural wax hydrophobic formulation can serve as a safe, non-toxic, and sustainable anti-fogging coating for clear PPEs compared to several commercial solutions.

1 **Durability and Physical Characterization of Anti-Fogging**
2 **Solution for 3D-Printed Clear Masks and Face Shields**

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15 **Keywords:** Face shields, Masks, Anti-fogging

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19 **ABSTRACT**

20 **Background.** The COVID-19 pandemic brought forth the crucial roles of personal protective
21 equipment (PPE) such as face masks and shields. Additive manufacturing with 3D printing enabled
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25 **Methods.** We used additive 3D printing to generate the testing apparatus for contact angle, sliding
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28 sliding angle, and transmittance. Further, the integrity of this surface following several disinfection
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32 a highly hydrophobic surface (contact angle $150.3 \pm 2.1^\circ$ and sliding angle $13.7 \pm 2.1^\circ$) with
33 maximal transmittance. The use of soap for disinfection resulted in the complete removal of the
34 anti-fogging coating, while Isopropyl Alcohol and gauze optimally maintained the integrity of the
35 coated surface. Finally, the contact surface testing apparatus generated a light touch (5000 N/m^2)
36 that demonstrated good integrity of the antifogging surface.

37 **Conclusions:** This study demonstrates that a simple natural wax hydrophobic formulation can
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39 commercial solutions.

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46 INTRODUCTION

47 The COVID-19 pandemic has had a significant toll on the public health, biomedical, and
48 financial aspects that have significantly changed society.(1,2) Among various healthcare services,
49 the presence of SARS-CoV in the nasal and upper respiratory tract presented significant challenges
50 for dentists and anesthetists. Clinical dentistry presented a significant challenge due to the
51 proximity and inherent aerosol-generating procedures.(3-5) The use of personal protection
52 equipment (PPE) such as face masks and face shields was integral in reducing the spread of
53 infections among the general population. (6) While dentistry routinely utilizes face masks, double
54 masking, and the highly protective N95, the shielding nature and the lack of face-to face exposure
55 further compounded the pandemic fear and anxiety in patients naturally apprehensive about their
56 dental visits. (7-9) Another major limitation of these masks is that they hinder effective
57 communication due to the lack of non-verbal cues such as facial expressions and lips movements.
58 (10-12) This is particularly challenging in patients with differently-abled hearing due to increased
59 signal-to-noise from the ambient noise in dental operatories. (13-16) The use of transparent masks
60 and face shields has been demonstrated to improve these limitations. (17)

61 Another major challenge during the early phase of the pandemic was the significant
62 disruption of the PPE supply chain requiring local innovations where additive manufacturing using
63 3D printing came to the forefront. (18-21) The ability to generate required quantities based on need
64 and additional customization for individual applications were significant advantages of this
65 approach. (22) Building on this, in collaboration with e-NABLE, a 3D printing community,
66 students at the University at Buffalo School of Dental Medicine generated transparent PPEs using
67 3D printing and vacuum casting. Among them, several custom designs were specifically generated
68 to accommodate commercially available dental loupes that are made available freely online.(23)
69 These clear masks and face shields were well accepted and generated much enthusiasm among
70 clinical users. Besides dentistry, another group of clinicians that notably adopted these clear PPEs
71 were the local speech and hearing-impaired clinics. However, an immediate limitation of this
72 approach reported by users was the fogging due to the moisture from regular breathing. This
73 essentially negated the advantage of the transparent nature of these masks and face shields and
74 presented additional hindrance of needing repetitive wipe-downs.

75 The commercially available anti-fogging solutions used for eyeglasses and car exteriors
76 contain polydimethylsiloxane and silica nanoparticles.(24) The long-term use of these solutions
77 was considered unsuitable due to their potential for skin irritation, and potential inhalation or
78 ingestion. Hence, we sought to identify a non-toxic, antifogging coating for the transparent masks
79 and face shields for long-term use. To design such a solution, specific design criteria needed to be
80 met. The surface of a water droplet is attracted to the bulk of the droplet due to cohesion which
81 results in their beading. The shape that a drop takes on a given surface depends on the surface
82 tension of the fluid and the physical characteristics of the surface. A surface-fluid interface is the
83 contact angle that measures the wettability of a surface. Contact angles can vary from hydrophilic
84 (less than or equal to 30°) to hydrophobic (greater than or equal to 120°), where the higher the
85 contact angle, the lower its wettability. (25) Another measure of the extent of moisture retention
86 on a surface is the sliding angle which is measured by tilting the surface with the solution bead to
87 determine the angle at which it rolls off. The more hydrophobic the surface, the higher the angle
88 of loss of fluid droplets.(26) Another key design aspect of the anti-fogging solution would be its
89 resistance to wear due to repeated skin surface contact during mask use. The ideal solution would
90 offer a thin, durable coating for daily use that would not need repetitive applications while
91 maintaining maximal transparency.

92 Natural products offer attractive non-toxic coatings. Prior studies have examined the
93 combination of cinnamon and nutmeg that produces high hydrophobicity.(27) Although both are
94 natural products, this paper utilized a organosilane-based alkyl and perfluorinated synthetic
95 chemical coatings that raised some toxicity concerns due to high cuprous oxide content. We drew
96 inspiration from the naturally occurring, extremely hydrophobic lotus leaves. These leaves expel
97 water easily due to their micro-structural features, termed papillae, that exude epicuticular waxes,
98 cutin.(28,29) Alternatively, Carnauba and beeswax have also high hydrophobicity that are
99 routinely used in the food service industry.(30) With their high hydrophobicity, these solutions on
100 food containers prevent waste by ensuring minimal food retention. However, there was a lack of
101 clarity in the concentrations used in these prior formulations and the resulting hydrophobicity. The
102 present study examined the different formulations of these two waxes together and evaluated the
103 contact angle, sliding angle, and transmittance. The optimized formulation was subjected to
104 durability testing with manual disinfectant procedures and long-term contact-wear testing.

105 MATERIALS AND METHODS

106 Formulation of anti-fogging solutions

107 Hydrophobic wax coatings were generated in acetone or methanol as solvents using
108 ultrasonication. Different ratios of carnauba wax to beeswax (both Sigma Aldrich, St. Louis, MO)
109 were employed namely 0.4375 g: 0.4375 g (1:1), 0.35 g: 0.525 g (1:1.5), 0.33 g: 0.66 g (1:2), 0.417
110 g: 0.834 g (1:2HC) were melted in a 50 ml plastic tube (Corning, Thermofisher Waltham, MA) in
111 a water bath. After the waxes had melted, 25 milliliters of either acetone or methanol (both Sigma
112 Aldrich, St. Louis, MO) were added, and the solution was emulsified immediately using a probe
113 ultrasonication (Q2000, QSonica, Newtown CT) at 90% amplitude for 3 minutes and transferred
114 into a 50 ml glass spray bottle.

115 Contact and Sliding Angle testing

116 Solutions were sprayed onto a 2 x 2-inch sheet of PETG at roughly a distance of 5 inches, spraying
117 10 times. After drying, the sheets of PETG were tested for contact angle, sliding angle, and
118 transmission. A custom contact and sliding angle device were generated based on commercially
119 available models using online CAD software (Onshape, PTC, Rockwell Automation, Boston MA).
120 The devices were printed using Polylactic acid (PLA) filament (Overture, Overture 3D
121 Technologies, Texas) on a i3 Prusa 3D printer (Prusa Research, Prague Czech Republic) (**Figs. 1**
122 **A - C**). The device included a slot for to hold a mobile phone to take digital pictures of the droplet.
123 After fixing the plastic surface to the platform, droplets of water were generated with a 3 ml syringe
124 and 14-gauge needle (to mimic humidity post-condensation on clear PPEs) and digital image were
125 captured for analysis (**Fig. 1 D**). The digital images were analyzed using the NIH ImageJ (ver.
126 1.53n) software. The sliding angle set up included a protractor to assess the angle at which the
127 droplet slides off. The platform was tilted slowly until the water droplet slid off, and the angle was
128 documented (**Fig. 1 E**). All studies were performed in performed in triplicate and repeated at least
129 twice.

130 Transmittance analysis

131 The laser apparatus consisted of a 650 nm diode laser (Weber Medical, Beverungen, Germany) at
132 10 mW/cm², and a sensor with power meter (both Thor Labs, Newton NJ) (**Fig. 1F**). The sheets
133 of PETG were placed on top of the power sensor, and transmission was assessed.

134 Optical clarity analysis

135 A sticker was placed on a bench and the sheets of PETG were placed over it. Digital pictures were
136 taken with a mobile phone camera. The coated sheets of PETG were compared with the uncoated
137 control and the visual clarity of the coatings was assessed.

138 Routine manual disinfection testing

139 The PETG coated surfaces were subjected to different solutions such as soap solution (10% v/v,
140 Dawn, Procter & Gamble, Cincinnati OH), Isopropyl alcohol (70%, Sigma Aldrich, St. Louis MO),
141 and water alone using paper towels (Uline, Milton ON), gauge (Henry Schein, New York, NY) or
142 microfibers (Magic Fiber, Miami FL). These disinfectants were applied ten times in a uniform,
143 lateral motion with manual pressure by a single operator. Disinfection wipes (Metrex, Orange CA)
144 were used in another group.

145 Coating Durability following contact wear testing

146 To simulate accelerated contact wear testing, a custom apparatus was designed to mimic skin
147 contact. Using the CAD software (Onshape, PTC, Rockwell Automation, Boston MA), a rotating
148 platform with spring-loaded bases was designed to apply suitable skin contact forces. (31-33) The
149 device was 3D printed with PLA filament (Overture, Overture 3D Technologies, Texas) on a i3
150 Prusa 3D printer (Prusa Research, Prague Czech Republic). The wheel was connected to a DC
151 Motor (Greartisan, Shenzhen Hotec, China) via a speed controller and a 9V battery which allowed
152 the motor to function up to 1000 RPMs. After the coated samples were mounted on the platforms,
153 the apparatus was positioned to allow the platforms to extend and retract using centrifugal force
154 while spinning, hitting a skin-equivalent surface (rough side of oil-treated leather) to simulate
155 contact. To simulate multiple skin contacts, the device was operated for 5 minutes, allowing each
156 platform to contact the wall about 5000 times for each sample to simulate 4 weeks of routine wear.
157 The contact force applied by the rotational, spring-loaded platform was measured with a digital
158 force probe (Baoshishan, China). Following the contact wear testing, samples were assessed for
159 changes in contact angle, sliding angle, transmittance and examined with topological analysis.

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162 **Topological analysis**

163 Scanning electron microscopy (SEM) analysis was performed to determine the topology and the
164 depth of the coating on the plastic sheet samples prior to and following wear testing. Samples were
165 sputter-coated (Cressington 108, Ted Pella Inc, Redding CA) with carbon for 120 seconds and
166 examined using SEM (Hitachi, S-4700, Japan) with a voltage of 2.0 kV at about 14.5 ± 0.4 mm
167 using secondary electron mode.

168 **Statistical Analysis**

169 Data was organized in Excel (Microsoft, Seattle WA) and presented as Means with standard
170 deviations. Data was subjected to a Student's T test or two-way analysis of variance (ANOVA)
171 among different treatments with Bonferroni's correction for multiple comparisons where
172 appropriate. A $p < 0.05$ was considered statistically significant.

173 **RESULTS**

174 **Formulation and Characterization of Anti-Fogging solutions**

175 We first examined different ratios of carnauba and beeswax in two solvents namely
176 Acetone and Ethanol to generate a homogenous solution (**Fig. 2A**). The contact angles of the
177 acetone-based solutions were higher than their methanol counterparts (**Figs. 2B** and **2C**). The
178 coating with the highest contact angle was the 1: 2 ratio in acetone solution with a mean contact
179 angle of 150.3 ± 2.1 °. This categorizes this surface coating as highly hydrophobic compared to
180 the other coatings and was significantly ($p < 0.05$) more hydrophobic than the uncoated plastic
181 surface. We also examined the higher concentrations (HC) at 1 : 2 ratio to inquire if the density
182 and hence, eventual coating concentration would affect these properties, but did not observe any
183 further significantly improved characteristics. As expected the sliding angle for this coating was
184 the lowest at 13.7 ± 2.1 ° which was significantly ($p < 0.05$) lower than the uncoated plastic surface
185 (**Figs. 2D** and **2E**). The transmittance of these formulation appears to vary with the concentration
186 of the beeswax component as lower amounts resulted in higher transmittance (**Figs. 2F** and **2G**).
187 The optical clarity was also assessed through the observation of the sticker through the coated
188 slides. The optical clarity decreased as the concentrations of the solutes increased as was expected.
189 The methanol-based formulations had a comparable degree of transmittance (0.41 to 0.33) than
190 the acetone (0.3 to 0.26) counterparts compared to control (uncoated 0.43 ± 0.02). Based on these

191 results, we decided to pursue the 1:2 carnauba to bee wax in acetone formulation for subsequent
192 studies.

193 **Effect of routine disinfection procedures on durability of antifogging solution**

194 The use of disinfectants is a necessary part of routine plastic mask and face shield use due
195 to the prominent aerosol generating dental procedures. (34-36) Next, we examined routine
196 disinfectant procedures employed in the dental office namely, soap, water, and 70% Isopropyl
197 Alcohol with paper towels, gauze, or microfiber, and disinfectant wipes. We noted a significant (p
198 < 0.05) reduction in the contact angle after all disinfection methods (**Fig. 3A**). Among all these
199 methods, Isopropyl Alcohol with gauze reduced the contact angle the least ($144.3 \pm 1.6^\circ$) while
200 soap made the surface most hydrophilic (wettable), removing the coating most effectively.
201 Concurrently, the sliding angle analysis showed a similar trend, increasing overall with all, but the
202 soap group, disinfection methods (**Fig. 3B**). The Isopropyl alcohol group showed the least change
203 and no statistically significant difference was noted when a paper towel was used. Interestingly,
204 the transmittance appeared to vary after individual disinfectant methods with some showing
205 increases while other showing significant decreases (**Fig. 3C**). The method of disinfection that
206 showed most increase in light transmission were the sterilizing wipes by themselves. The lowest
207 transmission was observed with Isopropyl Alcohol and soap with paper towels. Together, these
208 results suggest that using Isopropyl Alcohol with gauze is optimal for disinfection as it minimally
209 affects antifogging coating properties such as contact and sliding angle and transmission after
210 repeated use.

211 **Antifogging coating stability after contact wear testing**

212 Finally, we investigated the durability of the anti-fogging solutions as they would be
213 subjected to rigorous daily wear and tear during PPE use. We first created a simple rig to simulate
214 skin contact based on a 3D printed apparatus (**Fig. 4A and B**). The rig was designed as a rotating
215 platform that would result in a repetitive contact of the coated device with a stationary leather
216 surface. The pressure exerted by facemask on the nose bridge and chin contact has been assessed
217 to be 45 to 91 mm of Hg (6000-12,000 N/m²) (**Fig. 4C**). (31-33) The constant skin contact force
218 in our device was assessed to be 5000 N/m² that could be approximated to a repeated light skin
219 contact.

220 Following the simulated wear, the contact and sliding angle as well as transmittance was
221 assessed. We observed a significant reduction in contact angle ($133.3 \pm 1.5^\circ$) and concomitant
222 increase in the sliding angle ($23.7 \pm 1.5^\circ$) compared to the uncoated control surfaces. While
223 transmittance was not significantly different before and after wear simulation, there was a trend
224 towards reduced transmission. Topological analysis noted the wear simulation resulted in
225 significant accretions and scratches that likely contribute to the reduced light transmission
226 observed. These results indicate that due to reduction in coating characteristics by about 50% over
227 the simulated 4-week wear period, the coating will likely need to be replaced as often as every
228 other week to maintain optimal functions.

229

230 DISCUSSION

231 The COVID pandemic presented new challenges to healthcare with an urgent need for
232 innovations in disinfection approaches. The use of PPE was central in the attempts to mitigate the
233 spread of infection and a major part of the solution to mitigate the health crisis. The use of these
234 barriers continues to have an impact on both the psychological, and medical well-being of both the
235 patients and the healthcare professionals themselves.(37) The initial response to the pandemic
236 brought manufacturing and supply chain disruptions resulting in additive 3D printing enthusiasts
237 to offer custom, local solutions. Our team at the University at Buffalo focused on the transparent
238 PPE designs and dental loop attachments (**Fig. 5**). The condensation from breathing obscured the
239 functions of the clear PPEs that presented a major impasse to their use. This work was specifically
240 motivated to address this deterrent to routine clear PPE use.

241 We tested polyethylene terephthalate glycol (PETG). PETG is a commonly-used
242 thermoplastic with impact resistance, durability, ductility, chemical resistance properties well-
243 suited to this application. To generate an anti-fogging solution for our clear face shields and masks,
244 a major design challenge was the close proximity to nose and mouth.(38,39) We chose to pursue
245 natural waxes as the main ingredient as they provided a natural, non-toxic solution that has a well-
246 established track record of biological safety. (40) The other major component constituent was a
247 polar solvent to enhance miscibility and dispersion of these waxes. We chose to examine Acetone
248 and Ethanol in our formulation. The acetone formulation was superior in generating the most
249 hydrophobic product after spray coating. Our initial efforts at dissolving the waxes in Acetone

250 (boiling point of 55.5°C) by heating alone resulted in evaporation and non-uniform dissolution.
251 Hence, we chose to disperse the waxes via ultrasonication. Among the various formulations, the
252 most hydrophobic surface was generated by the 1 : 2 ratio (contact angle $150.3 \pm 2.1^\circ$) though the
253 other formulations were also strongly hydrophobic (contact angles 121 to 135°). We also examined
254 Methanol (boiling point of 148.5 °F) in the same volume that, in contrast, generated hydrophilic
255 surface coatings with all formulations (contact angles 34 to 82 °), but most prominently with the 1
256 : 2 at the higher concentration (contact angle $80.7 \pm 2.1^\circ$). Increasing the concentration in the
257 Methanol formulation (1 : 2 HC) appeared to impact the physical characteristics more than the
258 Acetone (1 : 2 HC) formulation that could be attributed to differential dissolution of the waxes and
259 subsequent homogeneity of the coating film. Among the two solvents examined, Methanol did not
260 enable a suitable anti-fogging formulation and hence, the 1: 2 formulation in Acetone was chosen
261 as an optimal anti-fogging solution. This may have been due to the fact that methanol has a higher
262 polarity than acetone that facilitates improved dispersibility of the non-polar wax compounds.

263 The use of surface disinfectants is an integral part of maintaining and reusing PPEs. This
264 is a sustainable and cost-effective practice that is routinely employed. A key design requirement
265 of the anti-fogging solution is durability with these disinfectant approaches. We observed that the
266 soap solution group consistently demonstrated complete removal of the anti-fogging solution.
267 While this desirable as a disinfectant approach to remove all potentially hazardous aerosols on
268 these PPEs, its amphiphilic nature allowing it to form micelles with the wax components of the
269 anti-fogging solution would deem it unsuitable. The removal of the anti-fogging solution with
270 these approaches could be attributed to the surfactant nature that interferes with the surface tension
271 of the water droplets. Another possibility is that the lipid-to-lipid interaction of the soap and the
272 waxes may inactivate the hydrophobic nature of the coating. The superior solubilizing ability of
273 isopropyl alcohol that may further smoothen the coating, reduce surface tension further or alter
274 drying times are areas of future investigations.

275 To investigate the durability of the anti-fogging coating, we generated a custom rig for
276 accelerated surface contact testing. The major design principle for this device was to generate a
277 PPE skin contact force. The reported PPE skin contact force to create a tight seal on the nose and
278 chin has been reported as 45 to 91 mm of Hg (6000-12,000 N/m²). (31-33) The force generated by
279 our rig was lower at 5000 N/m² and was intended to approximate light skin contact force in non-

280 fastened areas. This reflects routine surface contact during routine use of the PPEs. The
281 hydrophobicity of the anti-fogging surfaces was relatively well maintained (contact angle $133.3 \pm$
282 1.5° and sliding angle $23.7 \pm 1.5^\circ$). However, the durability testing noted a reduction in the
283 transmittance of the masks that could be attributed the wear from the contact forces. As evident in
284 the ultrastructural analysis, the PETG surface appears to have several accretions and disruption of
285 the uniform coated surfaces. Given these PPEs are disposable and have a limited time of use, this
286 may not significantly impact the PPE performance. In fact, this lack of clarity from routine use
287 may be a good marker for replacement with a simple optical interferometry device.

288 This study has a few limitations. First, the biological performance of this anti-fogging
289 solution could be examined using *in vitro* (reconstructed human epidermis), and *in vivo* skin
290 contact testing in animals and human studies. (41-47) While this could be considered routine
291 diligence, it is prudent to emphasize both the waxes and PETG are generally regarded as safe (FDA
292 GRAS) and are used in current product (e.g; lip balm) formulations routinely. The solvents are
293 readily eliminated by mild heating (40°C overnight). Second, applying a hydrophobic solution on
294 the PETG clear surface may, counter to its primary objective, worsen the visibility due to the
295 moisture coalescing into larger water beads. It is conceivable that the increasing size of these water
296 beads may eventually reach a critical mass and cause them to slide off. This phenomenon is
297 observed on hydrophobic surfaces like lotus leaves and commercial car wax coatings. Hence, a
298 replaceable absorbent liner and a mild, mechanical vibration module to promote water droplet
299 beading and run-off could be attractive future design iteration in these clear PPEs. Third, a major
300 shortcoming of using such an anti-fogging spray is its temporary nature and the need for
301 continuous replacement throughout the lifetime of the clear PPE. Thus, a potential future
302 possibility is to pursue nanopatterning, simulating the lotus leaf papillae for a more biocompatible,
303 permanent anti-fogging solution.

304 **Conclusions**

305 In summary, this work demonstrates the utility of an anti-fogging formulation with two
306 natural waxes that has good durability and optimal non-fouling properties. This solution represents
307 a cost-effective, durable, non-toxic approach to prevent or reduce fogging of clear PPEs such as
308 plastic masks and face shields from condensations of humidity arising from breathing and
309 speaking.

310 **Conflicts of Interests**

311 The authors declare they have no relevant conflicts of interest with this work.

312 **Acknowledgements**

313 We thank the members of the Buffalo3DPPE for their time and effort during the pandemic namely,
314 Kierra Bleyle, Preethi Singh, Jason Ciano, Savannah Tomaka, Jacob Graca, Hunter Rosa, Yianni
315 Savidis, Danielle Detwiler, Omer Hillel, and Georgia Kyriacou. We also thank the Buffalo Enable
316 (BE Mask) team for their valuable collaboration and technical assistance with 3D printing namely
317 Aaron Gorsline, Albert Titus, James Whitlock, Peter Elkin, Jeremy Simon, Jon Schull, Ben Rubin,
318 Kelly Cheadle, Pete Suffoletto, and Skip Meetze. We would like to thank Mr. Peter Bush, South
319 Campus Instrument core for assisting with the SEM analysis and Weber Medical laser for
320 providing their laser device. This work was supported by the BlueSky, University at Buffalo, and
321 Dean's fund, School of Dental Medicine.

322

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445 Figure Legends**446 Figure 1. Physical characterization of anti-fogging coating**

447 (A.) CAD of the contact angle apparatus for 3D printing (B.) CAD of the sliding angle module for
448 3D printing (C.) 3D printed models of contact and sliding angle testing apparatus (D.) Image of
449 the contact angle assessment showing droplet generation and analysis. Inset shows the digital
450 analysis of contact angle ϕ using NIH ImageJ (E.) Digital image analysis showing the sliding angle
451 measurement using NIH ImageJ (F.) transmittance set-up using a diode laser and optical power
452 meter with the sensor.

453 Figure 2. Anti-fogging solution formulation and characterization

454 (A.) Tabular outline of the formulation depicting ratios of carnauba and beeswax in acetone and
455 methanol used to coat PETG plastic sheets (B. and C.) Contact angle assessment of Acetone and
456 Methanol formulations at various concentrations (D and E) Sliding angle analysis of Acetone and
457 Methanol formulations at various concentrations (F and G) Transmission of diode laser for
458 transmittance assessment of Acetone and Methanol formulations at various concentrations. (I.)
459 Digital image of an uncoated, Acetone and Methanol formulations applied to the PETG sheet. Data
460 are shown as Mean and SD and representative of at least two independent studies. Statistical
461 significance was determined using two-way analysis of variance (ANOVA) among different
462 treatments using Bonferroni's multiple comparison test ($n = 3$). Statistical significance is denoted
463 as * $p < 0.05$, ** $p < 0.005$, and *** $p < 0.0005$.

464 Figure 3. Effects of Disinfection on anti-fogging coating integrity

465 (A.) Contact angle assessment after various disinfection procedures (B.) Sliding angle analysis
466 after various disinfection procedures (C.) transmittance after various disinfection procedures. Data
467 are shown as Mean and SD and representative of at least two independent studies. Statistical

468 significance was determined using two-way analysis of variance (ANOVA) among different
469 treatments using Bonferroni's multiple comparison test ($n = 3$). Statistical significance is denoted
470 as * $p < 0.05$, ** $p < 0.005$, *** $p < 0.0005$, and **** $p < 0.00005$.

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473 **Figure 4. Durability testing of anti-fogging coating following contact testing**

474 (A.) CAD of contact testing apparatus used for wear testing analysis (B.) 3D printed model of the
475 assembled contact testing apparatus (C.) Outline of the eminent forces determining the contact
476 force on PETG surfaces. The contact angle (D.), sliding angle (E.), and transmittance (F.) analysis
477 before and after contact testing (G.) Scanning electron microscopy images of the uncoated and
478 coated surfaces before and after contact testing. Data are shown as Mean and SD and representative
479 of at least two independent studies. Statistical significance was determined using the Students' T-
480 test ($n = 3$). Statistical significance is denoted as * $p < 0.05$.

481

482 **Figure 5. Clear face shields and masks**

483 A clear mask design with filter unit in medium (A.) and large (B.) sizes. The 3D printed clear face
484 shields are shown to accommodate different dental operating loupes such as Eclipse (C.), Vision,
485 Surgitel and Orascoptic (D.). Images are provided with consent from lab volunteers from the
486 website www.buffalo3dppe.com.

Figure 1

Figure 1. Physical characterization of anti-fogging coating

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Fig. 1

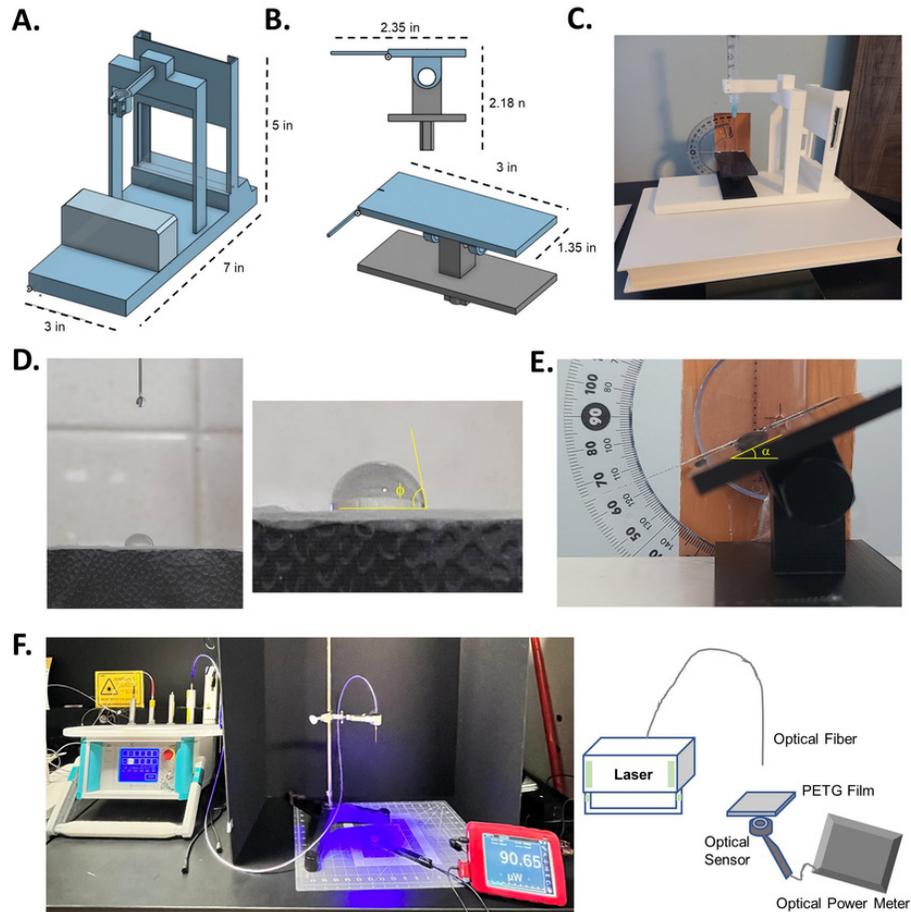


Figure 2

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Fig. 2

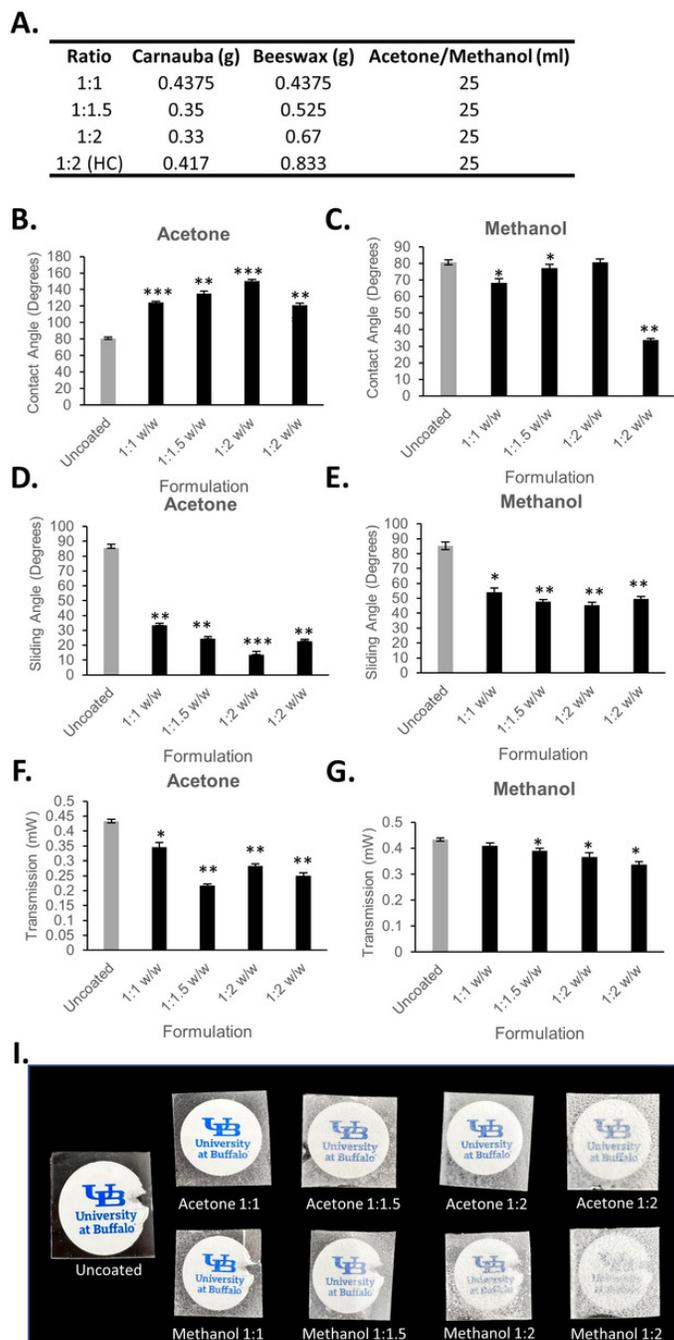


Figure 3

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Fig. 3

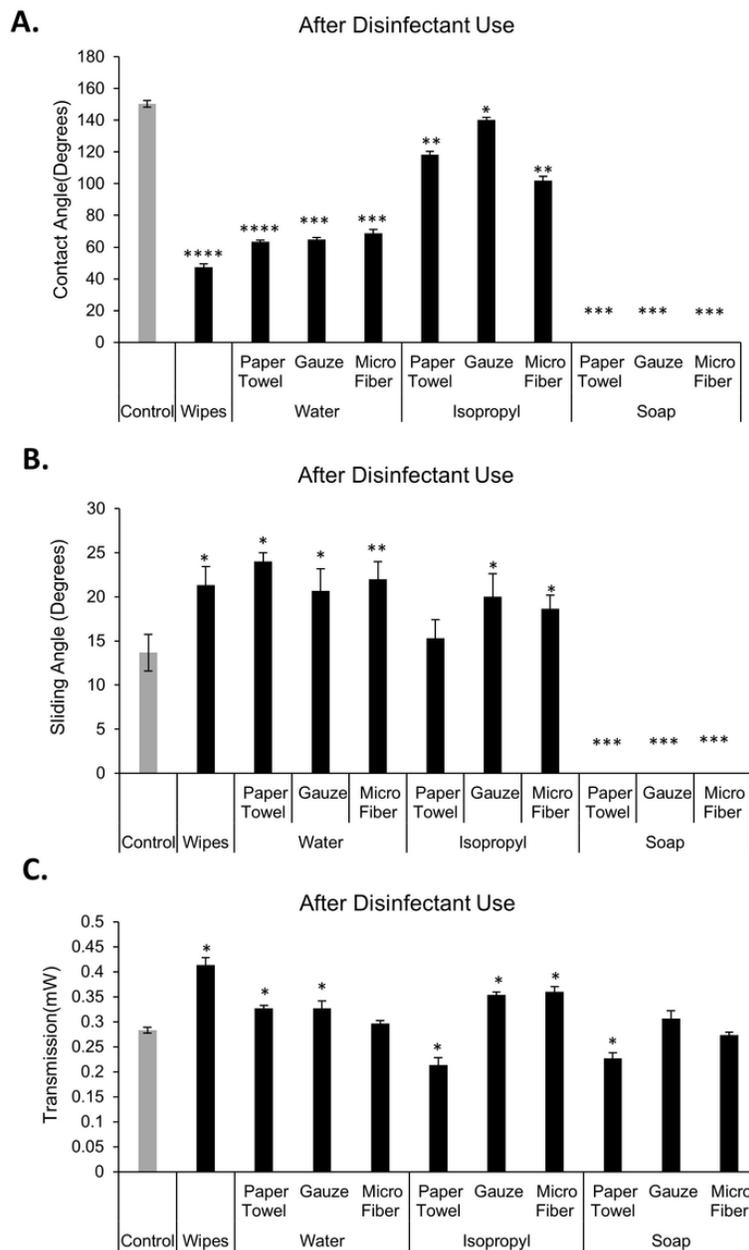


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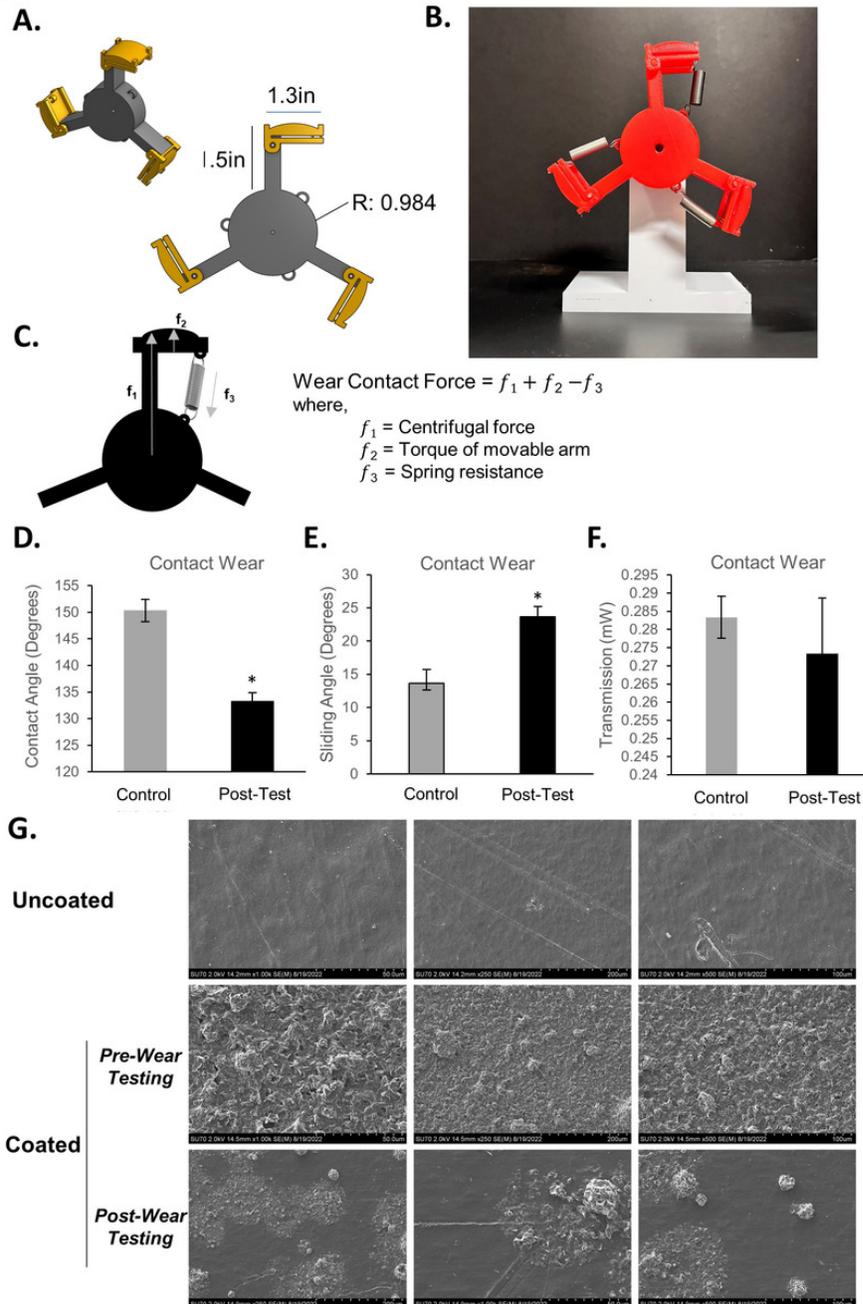


Figure 5

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Fig. 5

