The efficacy of computed tomography scanning versus surface scanning in 3D finite element analysis (#71965)

First revision

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The efficacy of computed tomography scanning versus surface scanning in 3D finite element analysis

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Finite element analysis (FEA) is a commonly used application in biomechanical studies of both extant and fossil taxa to assess stress and strain in solid structures such as bone. FEA can be performed on 3D structures that are generated using various methods, including computed tomography (CT) scans and surface scans. While previous palaeobiological studies have used both CT scanned models and surface scanned models, little research has evaluated to what degree FE results may vary when CT scans and surface scans of the same object are compared. Surface scans do not preserve the internal geometry of 3D structures, which are typically preserved in CT scans. Here, we created 3D models from CT scans and surface scans of the same specimens (crania and mandibles of a Nile crocodile, a green sea turtle, and a monitor lizard) and performed FEA under identical loading parameters. It was found that once surface scanned models are solidified, they output stress and strain distributions and model deformations comparable to their CT scanned counterparts, though differing by notable stress and strain magnitudes in some cases, depending on morphology of the specimen and the degree of reconstruction applied. Despite similarities in overall mechanical behaviour, surface scanned models can differ in exterior shape compared to CT scanned models due to inaccuracies that can occur during scanning and reconstruction, resulting in local differences in stress distribution. Solid-fill surface scanned models generally output lower stresses compared to CT scanned models due to their compact interiors, which must be accounted for in studies that use both types of scans.



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versus surface scanning in 3D finite element analysis

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Abstract

34 Finite element analysis (FEA) is a commonly used application in biomechanical studies of both 35 extant and fossil taxa to assess stress and strain in solid structures such as bone. FEA can be 36 performed on 3D structures that are generated using various methods, including computed 37 tomography (CT) scans and surface scans. While previous palaeobiological studies have used 38 both CT scanned models and surface scanned models, little research has evaluated to what 39 degree FE results may vary when CT scans and surface scans of the same object are compared. 40 Surface scans do not preserve the internal geometry of 3D structures, which are typically 41 preserved in CT scans. Here, we created 3D models from CT scans and surface scans of the same 42 specimens (crania and mandibles of a Nile crocodile, a green sea turtle, and a monitor lizard) and 43 performed FEA under identical loading parameters. It was found that once surface scanned 44 models are solidified, they output stress and strain distributions and model deformations 45 comparable to their CT scanned counterparts, though differing by notable stress and strain 46 magnitudes in some cases, depending on morphology of the specimen and the degree of 47 reconstruction applied. Despite similarities in overall mechanical behaviour, surface scanned 48 models can differ in exterior shape compared to CT scanned models due to inaccuracies that can 49 occur during scanning and reconstruction, resulting in local differences in stress distribution. Solid-fill surface scanned models generally output lower stresses compared to CT scanned 50 51 models due to their compact interiors, which must be accounted for in studies that use both types 52 of scans.

Introduction

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Finite element analysis (FEA) is a computational technique that reconstructs stress, strain, and deformation in solid structures. While initially common in engineering, architecture, and orthopaedic sciences, it is now widely used to assess the biomechanics of the human



57	musculoskeletal system and in recent years it has been a crucial tool in understanding vertebrate
58	biomechanics and evolution (Ross 2005; Rayfield 2007). FEA has been used in studies of 2D
59	(Rayfield 2004, 2005; Pierce et al. 2008; Pierce et al. 2009; Fletcher et al. 2010; Ma et al. 2021)
60	and 3D structures (Moreno et al. 2008; Bell et al. 2009 Oldfield et al. 2011; Cost et al. 2019;
61	Rowe & Snively 2021) to assess patterns and magnitudes of stresses and strain in both extant and
62	extinct organisms, as well as suture morphology in the crania of reptiles (Rayfield 2005; Jones et
63	al. 2017) and mammals (Bright & Gröning 2011; Bright 2012). While studies involving FEA
64	studies commonly focus on stress and strain occurring in the skull during feeding, studies may
65	also examine the biomechanics of other vertebrate appendages (Arbour & Snively 2009;
66	Lautenschlager 2014; Bishop et al. 2018).
67	FEA is popular in studies of fossil taxa as it is a non-destructive and non-invasive method to
68	study the structural mechanics of extinct organisms. These studies are sometimes conducted
69	using geometrically accurate 3D models which are generated through various techniques,
70	including photogrammetry (Falkingham 2012), computed tomography (CT) scanning and surface
71	scanning (Rayfield 2007). While CT scanning has seen common use in zoological and
72	palaeobiological studies involving skulls, surface scanning methods have often been used to
73	study fossil vertebrate morphology with 3D geometric morphometrics (Friess, 2006; Harcourt-
74	Smith et al. 2008; Kuzminsky et al. 2016). Surface scanning has also been used to study
75	locomotion via trackway scanning (Bates et al. 2008; Ziegler et al. 2020), and to scan immovable
76	museum specimens (Bates et al. 2009; Cunningham et al. 2014)
77	Computed tomography (CT) scanning
78	CT scans have an extensive history in the medical field (Power et al. 2016), but in recent decades
79	they have been commonly used in paleontological (Haubitz et al. 1988; Carlson et al. 2003;



80 Racicot 2016) and zoological studies (Copes et al. 2016; Poinapen et al. 2017). They allow for a non-invasive visualization of the interior of biological structures and can be used to generate 81 high resolution tomographic data of bone, fossils, and tissues. These data are used to create 3D 82 83 models which can facilitate biomechanical modelling, geometric morphometric analyses, or phylogenetic analyses. 84 85 CT scanning is a powerful tool in biological studies, as the 3D models generated from the scans 86 can capture both internal and external details with precision (Rowe et al. 2016). Image quality in 87 CT scans depends on four basic factors: image contrast, spatial resolution, image noise, and 88 artifacts (Goldman 2007), and can also vary by the size of the specimen being scanned and the type of machine used. While CT scanning offers many advantages, there are disadvantages 89 90 relative to surface scanning that must be considered, including high costs (Fred 2004), size 91 limitations, and time spent segmenting the data. Surface scanning and photogrammetry 92 93 Both surface scanning and photogrammetry are increasingly common digitization techniques 94 that have applications comparable to CT scanning (Remondino 2011). Like CT scanning, both 95 methods are used to generate virtual 3D data that can be valuable in biological studies. Surface scanning and photogrammetry may serve as alternative methods that avoid the expenses and 96 97 large size restrictions of CT scanning (Mallison et al. 2009), though the resulting 3D models 98 lack the internal anatomy of complex structures such as the endocast of the skull (Sutton et al. 99 2017). Since surface scans tend to miss intricate details of smaller specimens, e.g., bone textures 100 and teeth, CT scanning is generally the preferred method-when dealing with small specimens in 101 palaeobiological studies. However, not all specimens are amenable to CT scanning, due to their





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size, weight or accessibility, and surface scanning may offer a viable alternative (Cunningham et al. 2014). Laser scans and white light scans are two types of surface scans used in biological studies. Laser scanners use a one-dimensional type of scan with a line pattern, which may lead to a high error rate for certain objects (Persson et al. 2009). White light scanners use a two-dimensional stripe pattern for obtaining three-dimensional data. Generally, white light scanning is more accurate and faster in the scanning of plaster models in medical studies (Jeon et al. 2014); Peterson & Krippner (2019) found little difference in the effectiveness of one type of surface scan when comparing the fidelity of 3D printed teeth and osteoderms. Studies have already investigated which 3D scanning type is more reproducible in medical studies; Fahrni et al. (2017) concluded that multi-detector computed tomography (MDCT) led to greater variability in results when compared to three-dimensional surface scanning (3DSS) but noted that more experimentation was necessary to explain their first impression and expand on the results. Kulczyk et al. (2019) examined how cone-beam computed tomography (CBCT) scans compare to optical scans when comparing tooth models in 3D printing and found that highresolution CBCT is a sufficient method to obtain data, but the texture quality was poorer than in optical scan. Soodmand et al. (2018) examined the mean model deviation in CT data compared to reference optical 3D scans and found no significant discrepancies in 3D models of a human femur. Other studies have compared 3D models created via photogrammetry and CT scanning in contexts broader than medical studies. Lautenschlager (2016) noted that while photogrammetry is the most cost efficient and easily reproducible method, it can be limited in its applications due to its inability to capture internal geometries and complex surfaces. Fahlke & Autenrieth (2016) similarly noted that CT scanning has its main strength in capturing internal features, but surface



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scanning was otherwise sufficient in 3D model generation. Hamm et al. (2018) concluded that CT scanning was likely the better option for large, complex structures like a *Tyrannosaurus rex* skull, as the data-capture effort of photogrammetry is directly linked to the size and colour of the specimen and to the complexity of its shape. CT scanning is independent of the specimen's shape and complexity, with an accuracy and reproducibility of less than 1% mean error found in a previous study (Marcus et al. 2008) which can be advantageous in both time spent acquiring data and the quality of the models. While CT scanning and surface scanning have previously been compared in terms of topography and morphology (Waltenberger et al. 2021) and the efficiency of several different surface scanning methods have been compared in terms of digitization quality (Díez Díaz et al. 2021), little work has evaluated the downstream differences in finite element models created from CT scans versus surface scans. Particularly, little work has evaluated the possible discrepancies in 3D finite element results when comparing surface scanned models and CT scanned models derived from the same material. There is also little work investigating how to reduce possible discrepancies between results in 3D models generated from different scanning methods. Though the resolution of surface geometry and its influence on FE results has been studied (McCurry et al. 2015), this study is the first to evaluate the use of both CT scans and surface scans in 3D FEA. Primary hypotheses and rationale In this study we investigate the comparable difference in stress and strain output data between finite element models of the same specimen and loading conditions, created either from white

light surface scanning or computed tomography methods. We assessed the FE results from 3D

models of three reptile skull specimens: a Nile crocodile (Crocodylus niloticus) (Figure 1), a



148	monitor lizard (Varanus salvator) (Figure 2), and a green sea turtle (Chelonia mydas) (Figure 3).
149	They were chosen for their morphological diversity, differences in feeding biomechanics, and
150	ready availability of muscle data in the literature, including insertions and muscle force
151	components. Crocodilians are noted for their akinetic skull properties due to possessing a
152	secondary palette (Ferguson 1981; Bailleul & Holliday 2017), which provides a contrast to
153	monitor lizards which possess a more flexible, kinetic skull lacking a secondary palette (Arnold
154	1998; Herrel et al. 2007; Handschuh et al. 2019). The green sea turtle was chosen as a means of
155	testing a beaked omnivorous animal (Arthur et al. 2008; Nishizawa et al. 2010) in contrast to
156	sharply toothed carnivores.
157	Each specimen was digitized using a Nikon XT H 225ST μ CT scanner and an Artec3D Space
158	Spider surface scanner. CT parameters were set to 225 kV, 449 mA, 101 W, 1.5 mm copper
159	filter, 0.5 s exposure time, reflection rotating target, 3141 projections, and 4 frames per
160	projection. Manufacturers specifications list the surface scanning 3D point accuracy to 0.05 mm
161	and the 3D resolution at 0.1 mm, but this depends on distance from the specimen to the scanner
162	and specimen size. It is unlikely such resolution was achieved in this study, due to the large
163	specimens needing to be scanned at a certain distance away. The surface scanner was connected
164	to a Dell Alienware 13 Core i7-6500U laptop with 16 GB of RAM for processing complex
165	images. 3D models were created as STL files, because they are simple to work with and
166	supported by the majority of 3D visualization and editing software packages (Sutton et al. 2001).
167	Null hypotheses (1). 3D stress and strain magnitudes and patterns of stress for both the
168	CT scanned models and surface scanned models will be identical when they are analysed with
169	identical boundary conditions and material properties.



Alternative hypotheses (2). 3D stress and strain magnitudes and patterns of stress will 170 vary between CT scanned models and surface scanned models when they are analysed with 171 172 identical boundary conditions and material properties. We predict that surface scanned models experience lower stress and strain due to possessing dense internal geometries that are 173 174 reconstructed in model editing software, while CT scanned models possess geometrically 175 accurate interiors containing more hollow space. These hypotheses relate to the stress and strain of 3D skeletal structures when scanned using two 176 177 different methods. Stress is a physical quantity that expresses the internal forces that neighbouring particles of a material exert on each other, and strain is the measure of the 178 179 material's deformation when a stress is applied. The skull models were primarily compared by 180 mean von Mises stress (von Mises, 1913), a value which accurately predicts how close ductile (slightly deformable/non-brittle) materials like bone are to their failure point. Skull models with 181 lower von Mises stress were judged to be stronger under the imposed bite simulations, as lower 182 183 stresses indicate less susceptibility to breakage or deformation under the imposed load. **Materials & Methods** 184 Scanning procedures 185 186 We created 3D models of the crania and mandibles of three phylogenetically disparate taxa using both CT scanning and surface scanning. These specimens include a Nile crocodile (BRSUG 187 188 28959), a monitor lizard (BRSUG 29376/7), and a green sea turtle (Ost 160). The reptiles are 189 housed in the University of Bristol Geology collection (BRSUG) or the University of Bristol, School of Biological Sciences teaching collection (Ost/H1b). The Nile crocodile skull was 190 191 selected for its relatively large size which enabled easier surface scanning, as intricate details 192 including wrinkled textures and teeth are often difficult to capture when scanning small

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specimens. This specimen possesses fibrous tissues in its cranium and mandible which were
captured during CT scanning and surface scanning, which may present a potential issue when
surface scanning extant osteological material. This is due to fibrous tissues potentially leading to
the creation of unrealistically large surfaces on the model, whereas the CT scanning preserves
the intricate details without unrealistically enlarging the surface. The Nile crocodile was missing
the posterior part of the left mandible and the Varanus salvator specimen was missing the entire
right mandible and the right maxilla and jugal were displaced from the cranium. This meant that
element duplication and minor restoration was required.
All reptile specimens were scanned using a Nikon XT H 225ST μ CT housed in the Life Sciences
Building, Bristol, UK. Due to the size of the adult crocodile skull, the cranium and mandible
were scanned separately, while the turtle and monitor lizard were scanned with both the crania
and mandibles held together by foam. All specimens were scanned at 120 μm . The files were
imported into Avizo Lite version 9.7 at voxel dimensions 1-1-1 to match the native scan
resolution and then segmented using only the Threshold tool. CT scanned models were scaled in
MeshLab 2020.03 to adjust length and width dimensions to their surface scanned counterparts as
needed. These models were then exported as the STL file type.
The same CT scanned individuals were surface scanned using an Artec Space Spider handheld
scanner. The scans were made at 7-8 frames per second, with the 'real-time fusion' option
enabled. Real-time fusion aids in piecing together scans during the scanning process and may
save time when building the full model in Artec Studio Professional 14. Crania and mandibles
were all scanned separately and created as separate 3D object files to avoid both large file sizes
and intertwining crania and mandibles during surface scanning. CT scanning crania and
mandibles together, as was done with the turtle and lizard, is not an issue due to all internal



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details being captured separately. Additionally, the segmentation process post CT scanning can separate intertwining models. Surface scans were imported into Artec Studio 14 Professional where sections of scanned skulls were oriented together, registered, and then merged into a single object. Stray pixels were deleted, as well as frames with maximum error values above 0.3. Once we were satisfied with the alignment of the individual scans, we applied Global Registration to convert all one-frame surfaces to a single coordinate system using information on the mutual position of each surface pair. We were satisfied with our alignment once the scans were free of floating pixels and generally resembled the bones we scanned. We then applied a sharp fusion to create a polygonal 3D model, which solidifies the captured and processed frames into an STL file. We used Sharp Fusion rather than Fast Fusion or Smooth Fusion as it best preserves fine details of the scans, including small teeth and rugose bone textures, which were present in the crocodile skull. We then used the small-object filter to clean the STL file of any remaining floating pixels, which are inevitable in most surface scanning procedures. Additionally, we used the fix holes function to fill any open areas (Figure 4). The STL files were then exported from Artec Studio 14 Professional and imported into Blender version 2.82 for both surface editing and reconstruction of missing elements in the case of the crocodile and lizard mandibles, as well as the missing cranial elements of the lizard. 3D finite element model editing Blender 2.82 was used for more precise editing, typically using the Sculpt functions to smooth over any unnatural-looking surfaces or creases that tend to appear in surface scanned models. Most CT scanned models did not require extensive editing; they were run under Geomagic's Mesh Doctor function to remove self-intersections which often resulted after segmentation in



Avizo. Due to surface scanning producing hollow models, it was necessary to import the hollow
models into Avizo Lite 9.7 and segment them to achieve results comparable to the CT models.
This was done by converting the STL files into TIF files, segmenting the interior of the model
using Avizo's threshold tool, and generating a surface which was then exported as an STL. This
process fills in the entirety of the surface scanned models, leading to a denser interior than that of
the trabecular bone preserved in CT scans. We worked under the assumption that the dense
interior functions more similarly to the CT scanned models than leaving the models hollow, as
stated in our alternative hypothesis (2).
The interior details of surface scanned crania are generally not captured during scanning. In this
study, inner cranial details were constructed from observations of the CT scanned models. We
did this using the Sculpt function in Blender 2.82 for the turtle cranium, due to its dense, bony
skull (Figure 4). This-included the parietal and postorbital bones of the turtle, as they were
difficult to capture during surface scanning.
For the crocodile mandible, the posterior end of the left mandibular ramus was missing (Figure
1). This was fixed in Blender 2.82 by deleting the missing left mandibular ramus at the middle
point of the mandible and duplicating the right mandibular ramus. The right ramus was then
mirrored and reattached at the mandible's anterior to create a complete mandible. The right
ramus of the monitor lizard mandible was also missing (Figure 2), and an identical procedure
using the left rami was applied to generate a complete mandible. Additionally, the left maxillary
and jugal bones of the lizard's cranium were missing, and an identical duplication and mirroring
approach was used. This procedure was used for both the surface scanned models and the CT
scanned models to best achieve identical geometries for FE testing and avoid inconsistencies as
much as possible. The merging of duplicated geometries in the models resulted in intersecting



triangles, which generally causes meshing procedures to fail when creating finite element
meshes. This was fixed by importing models containing self-intersections into MeshLab,
deleting intersecting triangles, and then using the hole-filling function in Geomagic Studio 12.
Once our models were free of holes and intersecting triangles, the 3D models were imported into
Geomagic Studio 12. The mesh wizard tool was then selected, which corrects intersecting
triangles, sharp edges, and holes, thus reducing the likelihood of errors when meshing the
models. The remesh tool was used to help correct irregularly sized triangles in each model. Both
element and triangle counts were reduced using the decimate tool as to both shorten analysis
times in Abaqus (Table 1) and to aid in reducing intersecting triangles and sharp edges, which
are more common in high-element STLs. Volume and surface area for each 3D model was
recorded (Table 2).
The models were exported from Geomagic and imported into HyperMesh (Altair) as four-noded
tetrahedral elements. Properties were assigned to the various materials, including Young's
modulus, the material's stiffness, and Poisson's ratio, the deformation of the material in
directions perpendicular to the direction of loading. Alligator skull bone properties (Zapata et al.
2010; Porro et al. 2011) were assigned to both the crocodile and turtle (Table 3). Alligator bone
has been used previously as an extant analogue in turtle studies (Ferreira et al. 2020) and is thus
considered acceptable here. Lizard bone properties (Dutel et al. 2021) were assigned to the
monitor lizard (Table 3). All materials were treated as isotropic and homogeneous. As the main
purpose of the study was to compare differences in stress and strain results due to geometry, it
was considered acceptable to use these material property values.
Constraints were assigned at anterior tooth edges and at the beak in the case of the turtle skull to
simulate feeding loads. We chose anterior feeding constraints for each model rather than



posterior to best visualize von Mises stress occurring all throughout each model for comparative
purposes. Constraints were assigned to the hinges of the articular and quadrate to prevent the
model from freely floating. Three constraint points were selected per quadrate and articular hinge
for each model. Three degrees of freedom were selected for each analysis at X, Y, and Z. The
number of constraint points, typically three per tooth or beak, were kept consistent for each taxon
and type of scan (Figure 5).
Once satisfied with the constraint selection, these models were imported into Abaqus to
determine stress and strain in the crania and mandibles of the models. Muscle locations and the
nodes selected to represent muscle attachment and insertion were based on reconstructions of
muscle anatomy from Holliday (2009) for Crocodylus (Figure 6) and Varanus (Figure 7) and
Jones et al. (2012) for <i>Chelonia</i> (Figure 8) (Table 4). Each muscle body was assigned a local
coordinate system to simulate the direction of pull of the muscles on the crania and mandibles. A
single coordinate system per muscle was created. Muscle force components applied to the model
were calculated by dividing muscle force (N) by number of nodes selected per muscle (see
supplementary information).
Muscle force values were obtained from previous studies involving taxa that are phylogenetically
related to those used in this study, including Alligator mississippiensis (Porro et al. 2011; see
supplementary information) applied to Crocodylus niloticus and Varanus niloticus (Dutel et al.
2021) applied to Varanus salvator. Platysternon muscle force values were chosen as a proxy for
Chelonia mydas due to possessing the highest recorded values of extant turtles which may align
more closely with the relatively large Chelonia skull (Ferreira et al. 2020; S. Lautenschlager,
personal communication 2021). Once all constraints and nodes were applied across CT scanned
and surface scanned models, FE analyses were run under linear static assumptions, with



unchanging loads and material properties in the software Abaqus (Simulia). Stresses were
compared using von Mises stress, which is used to predict failure under ductile fracture, or
fracture characterized initially by plastic deformation, commonly occurring in the bone. Stresses
were superimposed on the models as contours with a user-specified range of colours to indicate
where stresses experienced are least and most substantial, with warmer colours such as red and
white signifying high stress, and cooler colours like blue and green representing low stress.
Additionally, we analysed von Mises stresses and deformation occurring at specific points on the
models. This was done by plotting ten points at similar locations on each CT scanned model and
its corresponding surface scan model. We then selected five nodes per point on each model and
calculated the mean von Mises stress value at each point (Table 5, 6, 7). This was done to better
understand stresses occurring at specific points on each CT scanned model and its corresponding
surface scanned counterpart. A similar method was applied to each point where an unscaled
mean displacement was calculated by selecting five nodes. This method revealed the amount of
deformation occurring in each model and to what quantitative extent each CT scanned model
was deforming when compared to the surface scanned models. Points were chosen to capture
both as many different bones of each skull as possible and to quantify deformation in both areas
of low and high stress on the FE heatmaps. We considered using random points, but there is a
risk of those points only landing on very low or high stress areas, and the test may be less
informative if not comparing a range of differently-stressed points.
Once we calculated mean von Mises stress values for all models, we also calculated the mesh-
weighted arithmetic mean (MWAM) von Mises stress value for each model using R (R Core
Team 2021). This method accounts for element size differences within non-uniform meshes and
has been used in previous biomechanical studies of vertebrate palaeobiology (Marcé-Nogué et al.

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331	2016; Morales-García et al. 2019; Ballell & Ferrón 2021). It can reduce discrepancies in von
332	Mises stress between CT scanned models and surface scanned models. The code is as follows:
333	Stressfile<-read.table("model_smises.txt",header = T)
334	Stressfile
335	Volumefile<-read.table("model_evol.txt",header=T)
336	Volumefile
337	Stress<-Stressfile\$SMises
338	Stress<-as.numeric(Stress)
339	length(Stress)
340	Volume<-Volumefile\$Evol
341	Volume<-as.numeric(Volume)
342	length(Volume)
343	StressVolume<-numeric(length = length(Stress))
344	for (i in 1:length(Stress)) {StressVolume[i]<-Stress[i]*Volume[i]}
345	MWAM<-SumArea<-mean(StressVolume)/mean(Volume)
346	Results
347	In most FE models, mean von Mises stress magnitudes were generally higher in the CT scanned
348	models than the surface scanned models. The CT scanned models which produced von Mises
349	stresses higher than the surface scanned models were the Crocodylus cranium and mandible,
350	Varanus cranium, and Chelonia cranium. The mean von Mises stresses differed overall by
351	85.76% between both types of models (Figure 9), though certain models differed significantly
352	while others were comparable in their results, such as the Chelonia mandibles. We also
353	calculated the median von Mises stress values for each model (Figure 10). Median von Mises
354	stress values did vary from the mean stress values, in that the <i>Varanus</i> and <i>Chelonia</i> cranial



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stresses were slightly higher in the surface scanned models. Mean maximum principal strain values similarly differed overall by 86.04% (Figure 11). Our data on stress, strain and deformation values at specific points in both models was consistent overall with our mean von Mises stress data for each model in that the data demonstrated comparative trends between models, despite differences in model topography. Similarly, our specific point analysis of the unscaled displacement values yielded consistent results, with models that had undergone extensive reconstructions differing the most in unscaled displacement and those with little reconstruction yielding comparative FE data. Calculating the mesh-weighted arithmetic mean (MWAM) values significantly reduced the incongruity between CT scanned and surface scanned model stresses, as they differed overall by an average of 35.55% (Figure 12) compared to the unweighted average 85.76% value. Crocodylus results The *Crocodylus* crania were two of the more consistent models in terms of surface geometry, von Mises stress results, deformation, and 3D model properties (Table 1, 2). The number of elements between the two model types differed by 11.42%. Mean unweighted von Mises stress differed by 61.37% and mesh-weighted von Mises stress differed by 82.62%. Maximum principal strain differed by 52.12%. Like many of our models, stress distributions were noted for appearing similar in both versions, despite stress magnitudes being inconsistent (Figure 13). Both models were deforming in similar ways as well (Figure 14); anterior torsion occurred in each model due to teeth and their constraints only present on the right maxilla. Our specific point mean von Mises stress values overall differed by 75.97% (Table 5) and the mean unscaled

displacement values overall differed by 15.27% (Figure 15; Table 6).



Stress, strain and deformation magnitudes in the *Crocodylus* mandible surface scan model deviated significantly from its CT scanned counterpart. We attribute this to the extensive reconstructions which occurred in both models to fix the missing left mandibular ramus in the specimen (Figure 1). Difficulty in producing an identical model twice, as well as the process of creating interior-filled surface scan models, resulted in high variability between models in terms of von Mises stress and topography. Mean unweighted von Mises stress differed by 194.43% and mesh-weighted von Mises stress differed by 23.33%. Max strain differed by 32.6%. Our specific point mean von Mises stress values overall differed by 32.55% (Table 5) and the mean unscaled displacement values overall differed by 114.51% (Figure 15; Table 6). However, like the *Crocodylus* cranium, stress distributions still appear consistent between the models, despite the stark contrast in mean von Mises stress magnitudes and differences in the topography of the models (Figure 13, 15).

Varanus results

The *Varanus* crania were two of the most consistent models in their geometry, von Mises stress distributions, and deformation. Mean unweighted von Mises stress differed by 21.14% and mesh-weighted von Mises stress differed by only 3.16%. Mean maximum principal strain differed by 29.5%. As in the other models, stress distributions were noted for their consistency throughout (Figure 16), with lower von Mises stress occurring in the surface scanned mandible due to thicker rami as a result of surface scan reconstructions. The CT scanned cranium generally yielded lower von Mises stress throughout, likely as a result of the cranial bones being more geometrically accurate in their robusticity. Our specific point mean von Mises stress values overall differed by 83.76% (Table 7) and the mean unscaled displacement values overall differed by 24.52% (Figure 17; Table 8). Deformation was more noticeable in the surface scanned model,



400 especially in the bones of the cranium that were not as dense as the CT scanned model (Figure 401 14). The Varanus mandible models were two of the most inconsistent in terms of von Mises stress 402 magnitude, deformation, and particularly maximum principal strain. This is likely a result of the 403 relatively extensive reconstructive work applied to both models due to the missing right ramus, 404 405 comparable to the Crocodylus mandible. Mean unweighted von Mises stress differed by 112.55% and mesh-weighted von Mises stress differed by 63.78%. Max strain differed by 406 407 199.99%. Our specific point mean von Mises stress values overall differed by 99.57% and the 408 mean unscaled displacement values overall differed by 136.95% (Figure 17; Table 8). Like the other models, stress distributions were noted for their consistency despite the models having the 409 410 highest unweighted von Mises stress and maximum strain differences. Chelonia results 411 412 The *Chelonia* crania were relatively consistent in their geometric reconstructions, though the 413 bony interior of the skull was difficult to accurately model in the surface scanned version (Figure 414 18). Mean unweighted von Mises stress differed by 106.73% and mesh-weighted von Mises 415 stress differed by 11.59%. Maximum principal strain differed by 187.25%. Our specific point mean von Mises stress values overall differed by 52.34% (Table 9) and the mean unscaled 416 displacement values overall differed by 85.15% (Figure 19; Table 10). Stresses in the surface 417 418 scanned model were more noticeable at the crown of the skull, due to the bony interior being better preserved in the CT scanned model and thus lessening the stresses occurring in bone-laden 419 areas of the model. 420 421 The *Chelonia* mandible models were notable as they differed the least out of all models in terms 422 of stress, strain, and deformity, due to the geometrically simple shape and small size requiring



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423 minimal reconstruction in both models (Figure 18, 19). Mean unweighted von Mises stress differed by 18.31% and mesh-weighted von Mises stress differed by 6.24%. Max strain differed 424 by 14.79%. Our specific point mean von Mises stress values overall differed by 38.42% (Table 425 9) and the mean unscaled displacement values overall differed by 40.77% (Figure 19; Table 10). 426 The pattern and intensity of deformation was visually identical in both models (Figure 14). 427 **Discussion** 129 This study demonstrated that 3D FE results can vary significantly between CT scanned models and surface scanned models, though the distributions of stress/strain occurring in both types of 430 models tends to be similar. We can infer from these results that through use of surface scans, the 431 432 mechanical attributes (overall stress and strain distribution, deformation patterns) of organisms 433 can be confidently studied. However, the magnitude of stress and strain experienced is more difficult to assess. Calculating the mesh-weighted arithmetic mean (MWAM) to correct for 434 435 element size can mitigate the differences between von Mises stresses in studies using both types of 3D models, as evidenced in our study. 436 Significance of reconstructions 438 As demonstrated by our *Crocodylus* and *Varanus* mandibles, 3D models which have undergone 439 extensive reconstruction tend to differ most significantly in von Mises stress and strain. This is 440 due to a greater likelihood of models created from surface scan-derived data and those based on CT scan data differing due to scanning procedures and reconstruction. The *Crocodylus* mandible was missing a portion of its left ramus, and the Varanus mandible was missing its right ramus in 442 443 its entirety, which necessitated the use of model editing software Blender 2.82 and Geomagic Studio 12 to duplicate the existing ramus, mirror it, and reattach it to the opposite side of the 444 jaws to complete the mandible. The *Crocodylus* mandible models experienced the greatest 445



446	discrepancies in von Mises stresses, which we attribute to the extensive editing procedures
447	including duplication and mirroring that can be difficult to precisely reproduce in separate
448	models. The presence of fibrous tissues in the Crocodylus crania and mandible also contributed
449	to inconsistencies in surface model generation, leading to further geometric differences between
450	the two models (Figure 15, 20). These reconstructive procedures tend to be common in
451	biomechanical studies of fossil specimens (Nieto et al. 2021), as most specimens are missing
452	details comparable to the missing bones in this study.
453	The left Varanus mandibular ramus was similarly duplicated and attached at the anterior
454	symphysis; however, the smaller size and geometric simplicity made the process of producing
455	more identical models easier than the Crocodylus mandible. We attribute the lower von Mises
456	stress occurring in the surface scanned mandible to thicker rami as a result of surface scan
457	reconstructions. The right maxillary and jugal bones of the Varanus cranium were similarly
458	duplicated and applied to complete the entire cranial model. The relatively low von Mises stress
459	discrepancies between these models may be due to the overall minimal reconstruction necessary
460	in fixing the skull.
461	Due to its relatively small size, simple geometry, and completeness, the <i>Chelonia</i> mandible
462	required the least extensive reconstruction efforts for both CT and surfaced scanned models. The
463	mandibles also exhibited the smallest discrepancies between model types in terms of von Mises
464	stress and principal strain. We attribute these similarities in FE output to the factors outlined
465	above, which are sharply contrasted by the Crocodylus and Varanus mandibles. Generally,
466	models which required the least amount of reconstruction yielded stress, strain, and deformation
467	results that did not deviate markedly between CT scanned and surface scanned versions.
468	However, model simplicity is not a strict requirement for stress and strain congruence, as evident



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in the Crocodylus cranium, which were the largest models by surface area and volume and the second largest in terms of element number but still relatively consistent in FE output. Even in models yielding significant differences in von Mises stress values, the mesh-weighted arithmetic mean (MWAM) was useful in reducing overall stress differences. When this correction is applied, only the *Crocodylus* cranium shows an increase in von Mises stress discrepancy. As the geometries of models created via different scanning methods will vary, these calculations are integral to studies assessing biomechanical attributes of different scan types. While this study addressed the question of reconstruction significance in broken and incomplete specimens, which is often the case in biomechanics studies of fossils, there remains the question of whether more complete and simple models could have been utilized first. These models could be used as proof of concept, and function in a similar study of CT scans and surface scans. We did not use these hypothetical perfect models, as this study is intended for biological specimens and such incongruences are generally unavoidable in biological studies, especially using fossils. Conclusions When their utility in 3D FEA studies is compared to CT scans, white light surface scans are effective in capturing deformation and stress and strain distributions. These aspects relate to overall mechanical behaviour and make surface scan models fine candidates for use in studies concerning questions of relatedness in biomechanical patterns. However, surface scans may have questionable results when analysing absolute magnitudes of stress and strain in 3D models. As demonstrated in this study, geometrically simple objects requiring minimal editing, such as the Chelonia mandible, will not differ much from their CT versions, especially when the MWAM is calculated. Complex objects requiring little editing, such as the *Crocodylus* skull, also produce comparable results between surface scan and 3D. Objects which require extensive reconstructions, such as the *Crocodylus* and *Varanus* mandible, will result in incongruent



493 absolute magnitudes, though the MWAM calculation still aids in bridging the gap between results. 494 495 Studies utilizing both types of scans should attempt to avoid using specimens requiring extensive reconstructive work if possible, e.g., those missing skeletal elements. When this is not possible, 496 497 extra care must be taken to ensure that reconstructions are as accurate as possible. MWAM 498 calculations are recommended for all comparative FEA studies attempting to compare stress magnitudes in different model types. 499 **Future work** 500 This study used surface scanned models that were solidified post-surface reconstruction using the 501 502 segmentation tools in Avizo Lite 9.7, as surface scanned models are initially hollow upon 503 creation in Artec Studio 14 Professional. A question remains concerning the validity of hollow 504 surface scanned models and how much they deviate from solidified models in terms of von Mises stress. Studies only requiring the exterior of 3D structures, such as geometric 505 506 morphometrics, benefit from the time saved in retaining the hollow interior of the models. 507 However, the results of hollow surface scanned models in FE studies and the degree to which 508 their FE output would differ from solid models is not well understood, von Mises stress 509 distributions in hollow models may be similarly worth considering. 510 This study quantified differences in FE output when comparing different 3D models under 511 identical parameters. One of the difficulties of this study was maintaining identical parameters in 512 both sets of models due to incongruences in model geometry, reconstructions, and muscle nodes. Future work may attempt to compare more geometrically simple models as to limit these 513 514 inconsistencies between model output. Geometry of our models was kept as consistent as 515 possible; however, variance between models including element count and volume is generally



516	impossible to avoid. Future work may also attempt to refine our results by applying more
517	biologically complex and accurate modeling, particularly making use of more recent muscle data
518	(Gignac & Erickson 2016; Sellers et al. 2017; Wilken et al. 2019).
519	We chose not to test simple models, as such models are generally unrealistic in biological
520	studies, and such work may veer more into mechanics rather than biology. The FE-models
521	presented here reflect the nature of the complex geometry of the skull, which does influence FE-
522	model outputs from CT versus surface scanned models. Additionally, the turtle mandible we
523	tested yielded the smallest discrepancies in von Mises stresses, and it is the most geometrically
524	simple structure in our study. Thus, we may infer that models with few inconsistencies will
525	output the most similar FE results.
526	As we noted in our study, the mesh-weighted arithmetic mean (MWAM) is a powerful method of
527	mitigating von Mises stress differences between CT scanned models and surface scanned
528	models. In all models apart from the Crocodylus cranium, the discrepancies in mean von Mises
529	stress were reduced. Future work may attempt to further assess the effectiveness of the MWAM
530	in biomechanical studies involving 3D models, particularly those using different types of scans.
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Figure 1

The Crocodylus niloticus skull (BRSUG 28959) used in the study.

Left to right: cranium in dorsal view, cranium in ventral view, and mandible in dorsal view. Note both the presence of fibrous tissues in the specimen and the broken left ramus in the mandible. Photos by A. Rowe.



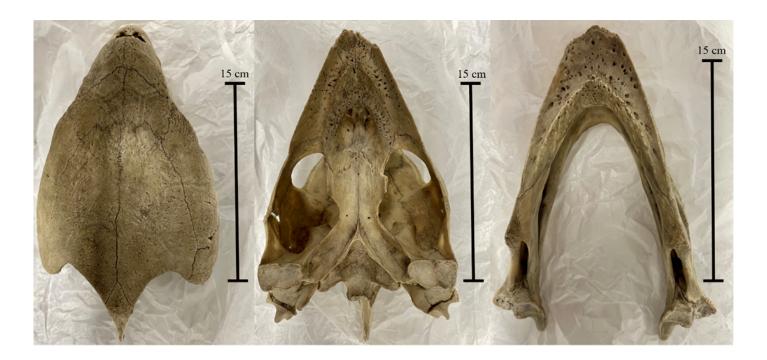
The Varanus salvator skull (BRSUG 29376/7) used in the study.

Left to right: cranium in dorsal view, cranium in ventral view, and the single left mandibular ramus in medial view. Note the partially broken right maxillary and jugal bones in the skulls. Photos by A. Rowe.



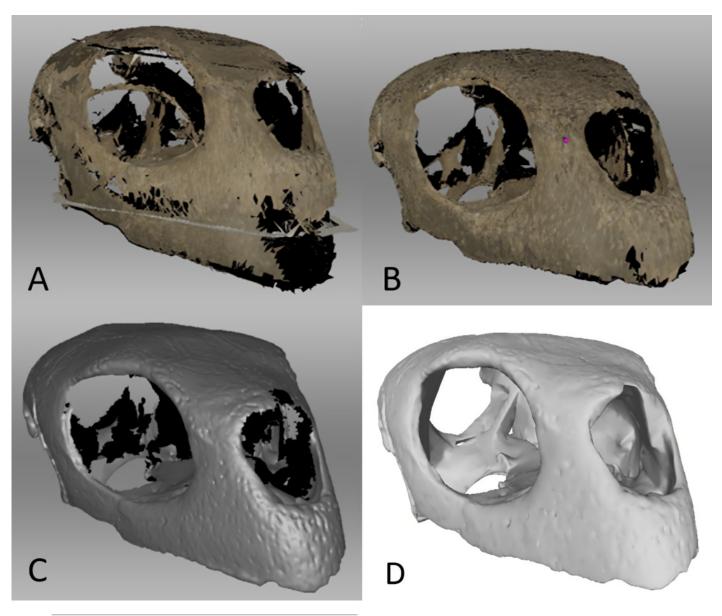
The *Chelonia mydas* skull (Ost 160 – Bristol Biological Sciences collection) used in the study.

Left to right: cranium in dorsal view, cranium in ventral view, and mandible in dorsal view. Photos by A. Rowe.



Surface scanned Chelonia cranium.

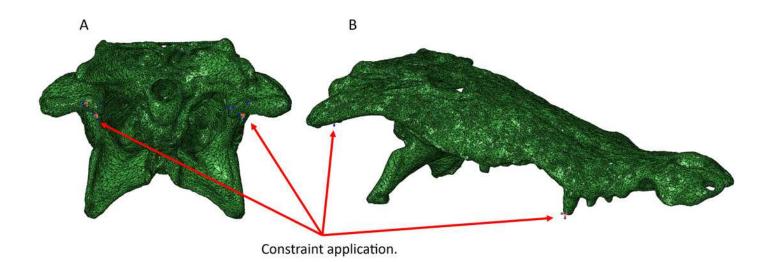
(A) Prior to Global Registration in Artec Studio 14 Professional, (B) after Global Registration and outlier removal in Artec Studio 14 Professional, (C) after Sharp Fusion in Artec Studio 14 Professional, which converts the scans into an STL file, and (D) the same STL file in MeshLab 2020.06 after surface editing in Artec Studio 14 Professional and Blender 2.82 to close gaps in the model and better match the geometry of the CT files.



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Areas of constraint application in the *Crocodylus* CT scanned cranium (A) in posterior view and (B) lateral view.

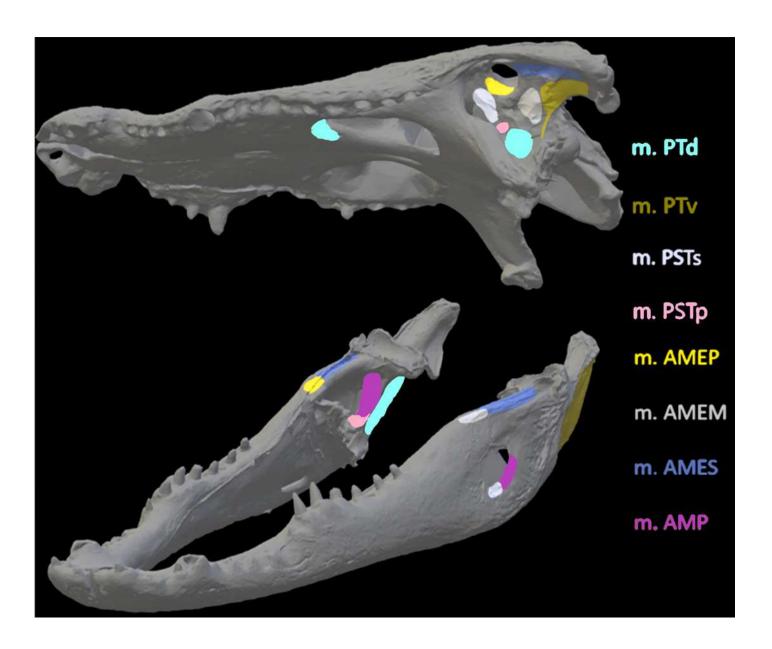
Three constraints were applied to each side of the quadrate to prevent the model from floating in space, and an additional constraint was applied to the anterior teeth to simulate contact with a food object. For mandible models, three constraints were applied to the posterior hinge of each articular bone. Identical constraint protocol was followed for each reptile model.



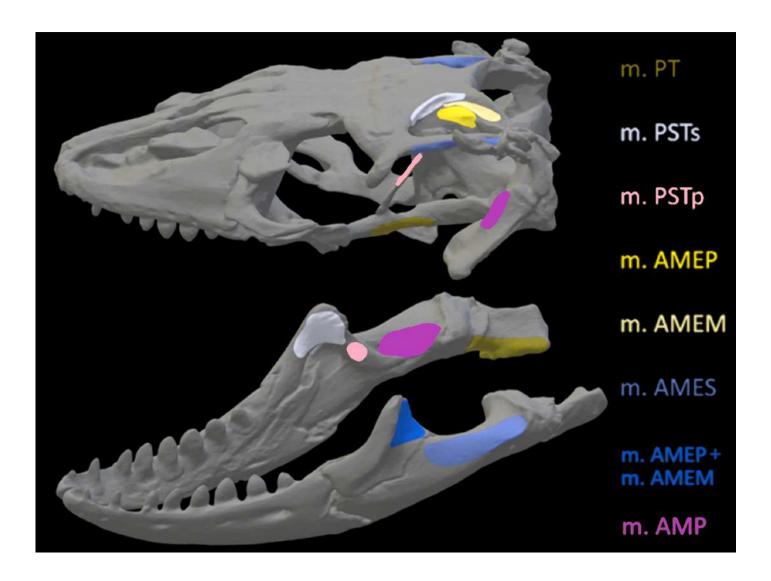


Muscle insertions where nodes were mapped for the *Crocodylus* model in Abaqus based on Holliday (2009).

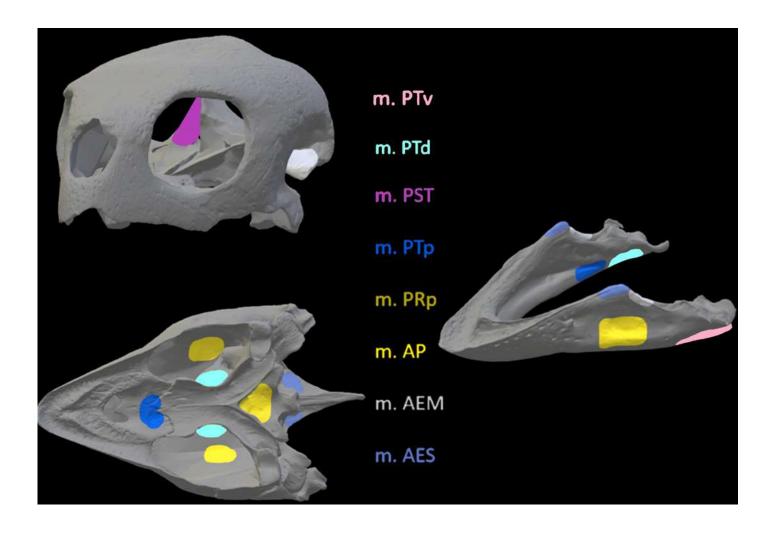
Nodes were mapped as similarly as possible for both CT scanned and surface scanned models by first applying nodes to CT models and then using the CT models as references when applying nodes to surface scanned models. Muscle abbreviations for all models: mPT, M. pterygoideus; mPSTs, M. pseudotemporalis superficialis; mPSTp, M. pseudotemporalis profundus; mAMEP, M. adductor mandibulae externus profundus; mAMEM, M. adductor mandibulae externus medialis; mAMES, M. adductor mandibulae externus superficialis; mPTd, M. pterygoideus dorsalis; mAMP, M. adductor mandibulae posterior; mPRp, M. adductor mandibulae internus Pars pterygoideus; mAP, M. adductor mandibulae externus Pars superficialis lateral head.



Muscle insertions where nodes were mapped for the *Varanus* model in Abaqus based on Holliday (2009).



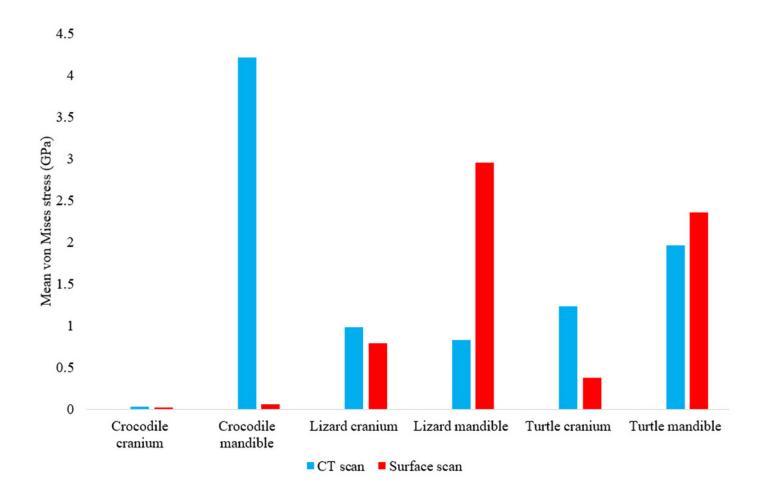
Muscle insertions where nodes were mapped for the *Chelonia* model in Abaqus based on Jones et al. (2012).



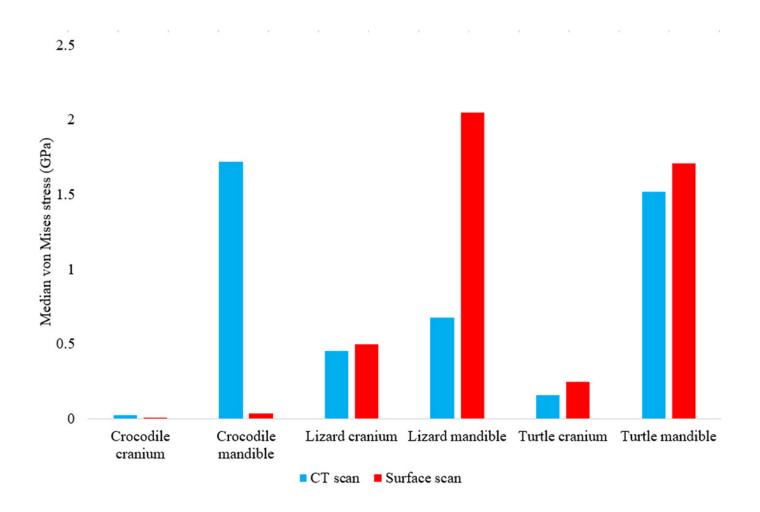


Mean unweighted von Mises stress values (GPa) in each FE model.

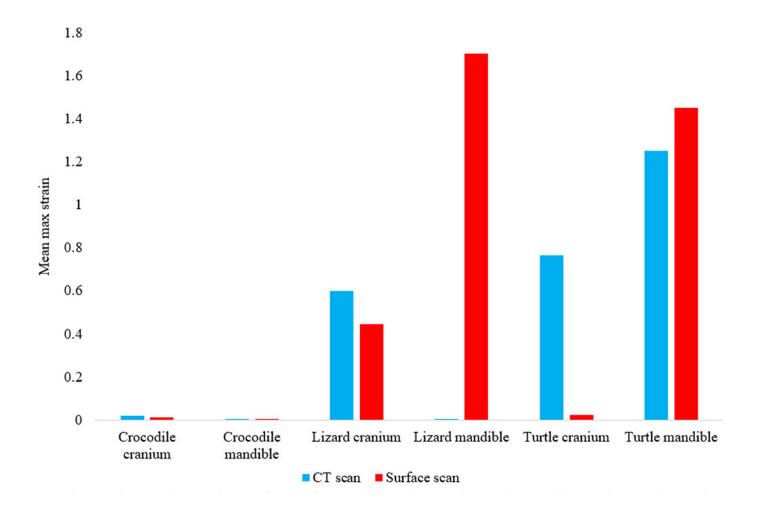
Note the large discrepancies in the models requiring more reconstructive work, i.e., the crocodile and monitor lizard mandibles.



Median unweighted von Mises stress values (GPa) in each FE model.



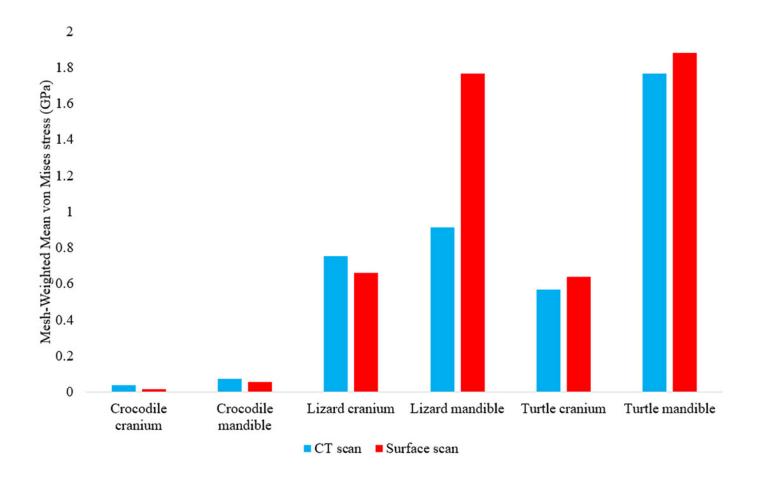
Maximum principal strain values (Emax) in each FE model. Y-axis represents the strain percentage.





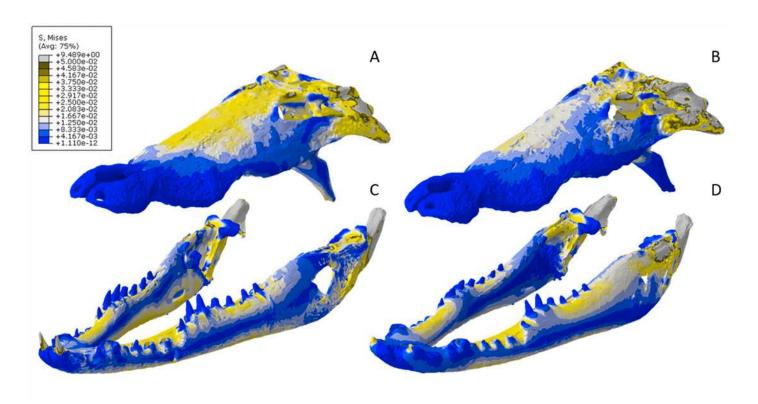
Mesh-weighted arithmetic mean (MWAM) von Mises stress values in each FE model.

Note the lower discrepancies in von Mises stress values between model types when the MWAM is calculated. This is further elaborated on in the Discussion section.



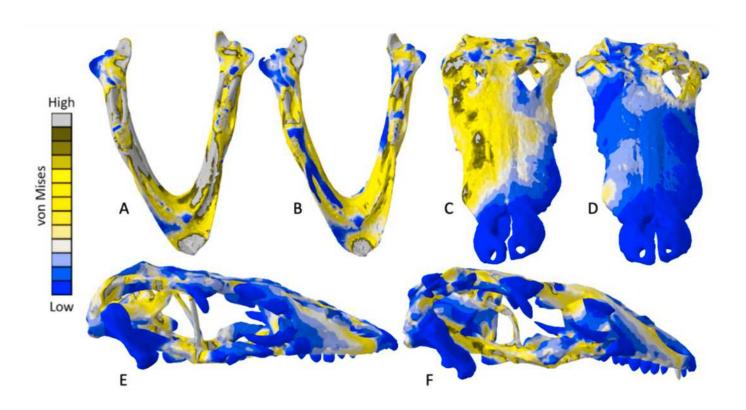
von Mises stress results for the Crocodylus models.

(A) CT scanned cranium, (B) surface scanned cranium, (C) CT scanned mandible, (D) and surface scanned mandible. Cooler colors like blue indicate low stress occurrences, while hotter colors such as orange indicate higher stresses. All FE model images were scaled to the same maximum stress values for consistency.



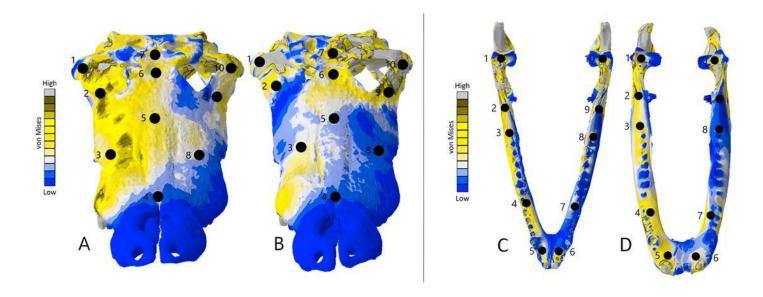
Exaggerated strain (Emax) deformation results in a selection of FE models tested.

(A) CT scanned *Chelonia* mandible, (B) surface scanned *Chelonia* mandible, (C) CT scanned *Crocodylus* cranium, (D) surface scanned *Crocodylus* cranium, (E) CT scanned *Varanus* cranium, (F) and surface scanned *Varanus* cranium. Magnification was at 75%. Models not to scale. Von mises stress key indicative of high and low values but not to scale across all models.



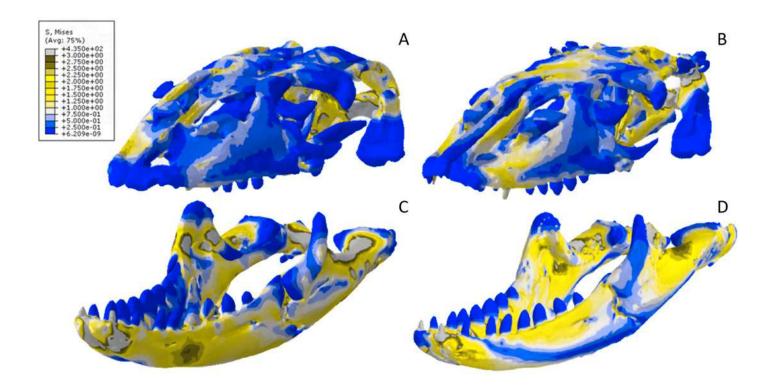
Dorsal view of the *Crocodylus* CT scanned cranium (A) and mandible (B) and surface scanned cranium (C) and mandible (D).

The mean von Mises stress of five nodes was recorded at each location, averaged, and documented in Table 8. Both FE model images were scaled to the same maximum stress values for consistency. The mean unscaled displacement of five elements to represent deformation was recorded at each point, averaged and documented in Table 7.



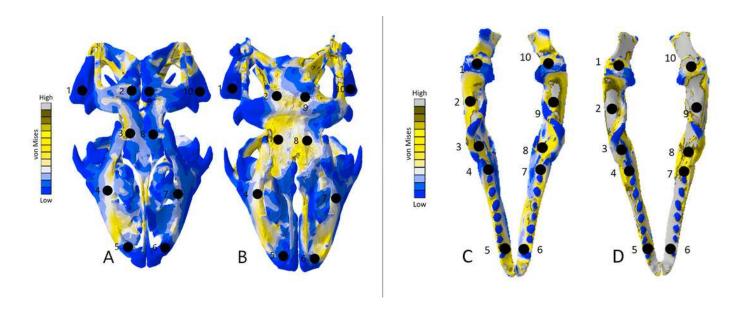
von Mises stress results for the Varanus models.

(A) CT scanned cranium, (B) surface scanned cranium, (C) CT scanned mandible, and (D) surface scanned mandible. All FE model images were scaled to the same maximum stress values for consistency.



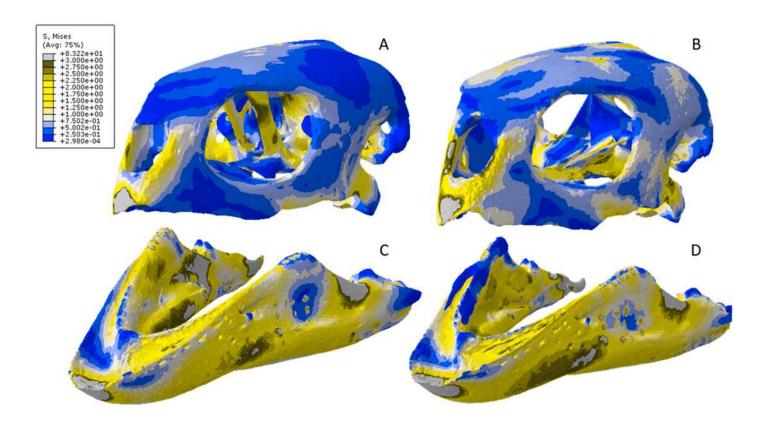
Dorsal view of the *Varanus* CT scanned cranium (A) and mandible (B) and surface scanned cranium (C) and mandible (D).

The mean von Mises stress of five elements was recorded at each location, averaged, and documented in Table 9. The mean unscaled displacement of five elements to represent deformation was recorded at each point, averaged and documented in Table 10. FE model images were scaled to the same maximum stress values for consistency.



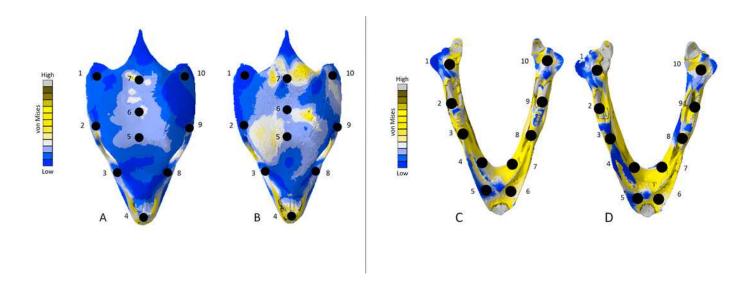
von Mises stress results for the Chelonia models.

(A) CT scanned cranium, (B) surface scanned cranium, (C) CT scanned mandible, and (D) surface scanned mandible. All FE model images were scaled to the same maximum stress values for consistency.



Dorsal view of the *Chelonia* CT scanned cranium (A) and mandible (B) and surface scanned cranium (C) and mandible (D).

The mean von Mises stress of five elements was calculated at each point and recorded in Table 11. The mean unscaled displacement of five elements to represent deformation was recorded at each point, averaged and documented in Table 12. FE model images were scaled to the same maximum stress value for consistency.



Dorsal view of the Nile crocodile mandible pinpointing areas of infilling during the surface scan reconstructions.

Fibrous material remaining on the mandible is the main cause of the surface scanned models being denser than the CT scanned version, as the infilling process connected fibrous tissues together and created a larger model than the CT version. This infilling process may also apply to extinct taxa where matrix may still be attached to the fossil rather than soft tissue.

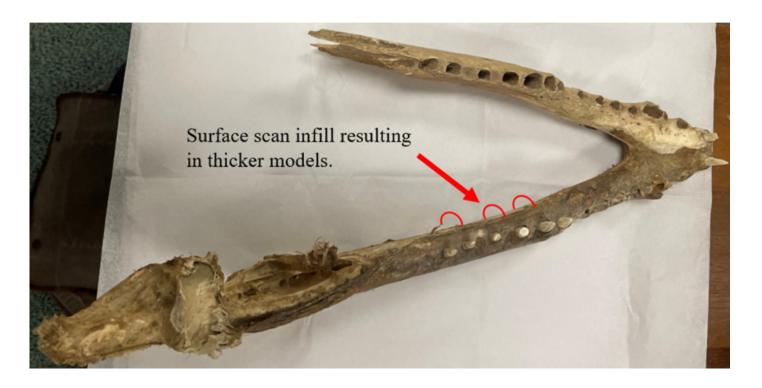




Table 1(on next page)

Number of elements and traingles in each model tested.

Specimen name	Cranial elements	Cranial element	s Mandible	Mandible	Cranial triangles Manuscript t	Cranial triangles o be reviewed	Mandible	Mandible
	(CT)	(surface scan)	elements (CT)	elements (surface		(surface scan)	triangles (CT)	triangles (surface
				scan)				scan)
Nile crocodile	1,386,928	1,554,868	2,019,264	1,801,958	167,940	217,306	1,386,928	247,090
(Crocodylus								
niloticus)								
Monitor lizard	159,358	172,470	688,656	135,450	159,358	172,470	588,656	135,450
(Varanus salvator	•)							
Green sea turtle	90,188	246,798	236,498	197,722	90,188	246,798	263,498	197,722
(Chelonia mydas)								



Table 2(on next page)

Volume and surface area of each model tested: volume is in cubic millimeters, and surface area is in square millimeters.

Specimen name	Cranial volume	Franjal yolume	Mandible volume	e Mandible volum	e Cranial surface Manuscript to	Cranial surface o be reviewed	Mandible surface	Mandible surface
	(mm^3) (CT)	(mm ³) (surface	(mm^3) (CT)	(mm ³) (surface	area (mm²) (CT)		area (mm²) (CT)	area (mm²)
		scan)		scan)		(surface scan)		(surface scan)
Nile crocodile	1256734.25	1716394.12	944250.68	1150979.75	346104.23	229887.71	285409.23	170483.37
(Crocodylus								
niloticus)								
Monitor lizard	23561.33	24318.68	7452.24	10201.48	22301.37	16554.88	8863.39	6507.72
(Varanus salvator))							
Green sea turtle	153623.06	173715.40	37029.62	34135.75	77998.11	67361.12	16474.20	14943.83
(Chelonia mydas)								



Table 3(on next page)

Material properties applied to 3D models.





Specimen name	Young's	Poisson's ratio
	modulus (GPa)	
Nile crocodile	15	0.29
(Crocodylus		
niloticus)		
Green sea turtle (Chelonia mydas)		0.4
Monitor lizard	22.8	0.3
(Varanus		
salvator)		



Table 4(on next page)

Number of constraints and muscle nodes applied to each model.

	Pee	erJ			Manuscript to k	oe reviewe	ed	
Total constrain	nts m. PTd	m. PTv	m. PSTs					MES m. AMP
at								
quadrate/articu	ılar							
6	16		27	10	28	14	27	27
6	54	52	32	32	47	38	62	80
6	16		23	10	24	14	28	24
6	49	51	30	28	27	41	60	70
	s m. PT	m. PSTs	m. PSTp	m. AMEP		AMES	m. AMP	
	nr				AIVIEIVI			
6	32	16	18	18	16 32		30	
6	42	32	10	18	16 38		34	
	at quadrate/articula 6 6 6 Total constraints at quadrate/articula	Total constraints m. PTd at quadrate/articular 6 16 6 54 6 16 Total constraints m. PT at quadrate/articular 6 32	at quadrate/articular 6 16 6 54 52 6 16 6 49 51 Total constraints m. PT m. PSTs at quadrate/articular 6 32 16	Total constraints m. PTd m. PTv m. PSTs at quadrate/articular 6 16 27 6 54 52 32 6 16 23 6 49 51 30 Total constraints m. PT m. PSTs m. PSTp at quadrate/articular 6 32 16 18	Total constraints m. PTd m. PTv m. PSTs m. PSTs at quadrate/articular 6 16 27 10 6 54 52 32 32 6 16 23 10 6 49 51 30 28 Total constraints m. PT at quadrate/articular 6 32 16 18 18 18	Total constraints m. PTd m. PTv m. PSTs m. PSTp m. AMEP at quadrate/articular 6 16 27 10 28 6 54 52 32 32 47 6 16 23 10 24 6 49 51 30 28 27 Total constraints m. PT m. PSTs m. PSTp m. AMEP m. AMEP + m. m. at AMEM quadrate/articular 6 32 16 18 18 16 32	Total constraints m. PTd m. PTv m. PSTs m. PSTp m. AMEP m. AT at quadrate/articular 6 16 27 10 28 14 6 54 52 32 32 32 47 38 6 16 23 10 24 14 6 49 51 30 28 27 41 Total constraints m. PT m. PSTs m. PSTp m. AMEP m. AMEP + m. m. AMES at AMEM quadrate/articular 6 32 16 18 18 18 16 32	Total constraints m. PTd m. PTv m. PSTs m. PSTp m. AMEP m. AMEM m. AMEM at quadrate/articular 6 16 27 10 28 14 27 6 54 52 32 32 32 47 38 62 6 49 51 30 28 27 41 60 Total constraints m. PT m. PSTs m. PSTp m. AMEP at AMEM 4 AMEM quadrate/articular 6 32 16 18 18 18 16 32 30

Surface scan	6	28	16	20	20	16	32	36	
Surface scan	6	40	31	10	26	26	36	38	
2									
Chelonia	Total constraints	s m. PTv	m. PTd	m. PST	m. PTp	m. PRp	m. AP	m. AEM	m. AES
	quadrate/articula	ar							
CT cranium	6		12	12	6	8	12	12	10
CT mandible	6	20	20		16		24	16	20
Surface scan	6		14	12	6	10	14	12	14
cranium									
Surface scan	6	20	22		16		22	16	20

mandible



Table 5(on next page)

Mean von Mises stress values (GPa) at locations 1-10 on Crocodylus FE models.



Point	Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus
	cranium	cranium	mandible	mandible	cranium	cranium	mandible	mandible
	CT scan	surface	CT scan	surface	model	model	stress	stress
	stress	scan stress	stress	scan stress	stress	stress	difference	difference
					difference	difference		percentage
						percentage		
1	0.068	0.093	0.09	0.233	-0.025	31.06%	-0.143	88.54%
2	0.063	0.013	0.095	0.112	0.05	131.58%	-0.017	16.43%
3	0.065	0.016	0.121	0.111	0.049	120.99%	0.01	8.62%
4	0.021	0.003	0.136	0.133	0.018	150%	0.003	2.23%
5	0.048	0.012	0.145	0.137	0.036	120%	0.008	5.67%
6	0.041	0.028	0.158	0.095	0.013	37.68%	0.063	49.80%
7	0.036	0.039	0.033	0.056	-0.003	8%	-0.023	51.69%
8	0.026	0.006	0.053	0.036	0.02	125%	0.017	38.20%
9	0.027	0.031	0.038	0.024	-0.004	13.79%	0.014	45.16%
10	0.062	0.077	0.151	0.183	-0.015	21.58%	-0.032	19.16%



Table 6(on next page)

Mean unscaled displacement values in cm at locations 1-10 on *Crocodylus* FE models. Mean values were calculated by recording and averaging five unscaled displacement values at each location as indicated on Figures 15 and 16.



Poi	nt Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus	Crocodylus
	cranium CT	cranium	mandible C	Γmandible	cranium	cranium	mandible	mandible
	displacemen	tsurface scan	displacemen	tsurface scan	model	model	displacemen	tdisplacement
		displacemen	nt	displacemen	tdisplacemen	tdisplacemen	tdifference	difference
					difference	difference		percentage
						percentage		
1	0.00289	0.00248	0.0412	0.0124	0.0004	15.27%	0.0288	107.46%
2	0.00384	0.00244	0.0553	0.0145	0.0014	44.59%	0.0408	116.91%
3	0.00430	0.00329	0.0861	0.0143	0.0010	26.61%	0.0718	143.03%
4	0.00525	0.00405	0.0936	0.0080	0.0012	25.81%	0.0856	168.61%
5	0.00448	0.00326	0.0509	0.0048	0.0012	31.52%	0.0461	165.53%
6	0.00347	0.00271	0.0214	0.0050	0.0008	24.60%	0.0164	124.86%
7	0.00276	0.00245	0.0341	0.0051	0.0003	11.90%	0.0290	147.87%
8	0.00495	0.00376	0.0316	0.0099	0.0011	27.32%	0.0217	104.51%
9	0.00384	0.00328	0.0263	0.0195	0.0006	15.73%	0.0068	29.69%
10	0.00290	0.00325	0.0192	0.0109	-0.0004	11.38%	0.0083	55.15%



Table 7(on next page)

Mean von Mises stress values (GPa) at locations 1-10 on Varanus FE models.



Point	Varanus	Varanus	Varanus	Varanus	Varanus	Varanus	Varanus	Varanus	
	cranium	cranium	mandible	mandible	cranium	cranium	mandible	mandible	
	CT scan	surface	CT scan	surface	model	model	stress	stress	
	stress	scan stress	s stress	scan stress	s stress	stress	difference	difference	
					difference	difference		percentage	
						percentage			
1	0.006	0.008	0.297	2.471	-0.002	28.57%	-2.174	157.08%	
2	0.425	0.927	2.256	4.714	-0.502	74.26%	-2.458	70.53%	
3	2.231	2.603	1.829	0.958	-0.372	15.39%	0.871	62.50%	
4	0.875	1.166	0.751	1.378	-0.291	28.52%	-0.627	58.90%	
5	0.699	0.056	0.038	3.756	0.643	170.33%	-3.718	195.99%	
6	0.091	0.605	0.031	8.552	-0.514	147.70%	-8.521	198.56%	
7	0.658	0.924	1.433	1.939	-0.266	33.63%	-0.506	30.01%	
8	0.523	1.002	2.421	2.612	0.479	62.82%	-0.191	7.59%	
9	0.025	1.128	2.885	5.116	-0.903	133.48%	-2.231	55.77%	
10	0.012	0.002	0.414	3.604	0.01	142.86%	-3.19	158.79%	



Table 8(on next page)

Mean unscaled displacement values in cm at location 1-10 on *Varanus* FE models. Mean values were calculated by taking the average of five unscaled displacement values at each location as indicated on Figures 13 and 14.



Po	int Varanus	Varanus	Varanus	Varanus	Varanus	Varanus	Varanus	Varanus
	cranium CT	cranium	mandible C	Γmandible	cranium	cranium	mandible	mandible
	displacemen	tsurface scan	displacemen	ntsurface scan	model	model	displacemen	tdisplacement
		displacemen	nt	displacemen	tdisplacemen	t displacemen	tdifference	difference
					difference	difference		percentage
						percentage		
1	0.0115	0.0016	0.0306	0.0373	0.0099	152.22%	-0.0067	19.73%
2	0.0092	0.0099	0.0327	0.0838	-0.0008	7.81%	-0.0511	87.73%
3	0.0131	0.0131	0.0329	0.1190	-0.0016	13.01%	-0.0861	113.36%
4	0.0156	0.0156	0.0279	0.1410	-0.0012	8%	-0.1131	133.93%
5	0.0144	0.0116	0.0102	0.1790	-0.0003	2.62%	-0.1688	178.44%
6	0.0133	0.0118	0.0080	0.1920	0.0005	4.15%	-0.1840	183.96%
7	0.0123	0.0127	0.0205	0.2140	-0.0003	2.39%	-0.1935	165.03%
8	0.0124	0.0128	0.0216	0.2620	-0.0015	12.45%	-0.2402	169.54%
9	0.0098	0.0105	0.0197	0.1860	-0.0007	6.39%	-0.1663	161.69%
10	0.0049	0.0034	0.0133	0.1080	0.00149	36.21%	-0.0947	156.14%



Table 9(on next page)

Mean von Mises stress values (GPa) at locations 1-10 on Chelonia FE models.



Point	Chelonia	Chelonia	Chelonia	Chelonia	Chelonia	Chelonia	Chelonia	Chelonia	
	cranium	cranium	mandible	mandible	cranium	cranium	mandible	mandible	
	CT scan	surface	CT scan	surface	model	model	stress	stress	
	stress	scan stress	s stress	scan stress	s stress	stress	difference	difference	
					difference	difference		percentage	
						percentage			
1	0.314	0.138	0.983	1.195	0.176	77.88%	-0.212	19.47%	
2	1.693	0.649	7.959	7.795	1.044	89.15%	0.164	2.08%	
3	0.818	1.029	3.814	1.156	-0.211	22.85%	2.658	106.96%	
4	0.651	0.935	1.539	0.869	-0.284	35.81%	0.67	55.65%	
5	0.659	0.669	0.985	1.379	-0.01	1.51%	-0.394	33.33%	
6	0.871	0.731	2.403	1.464	0.14	17.48%	0.939	48.56%	
7	0.564	1.124	3.191	3.572	0.56	66.35%	-0.381	11.27%	
8	0.456	0.802	2.648	2.263	-0.346	55.01%	0.385	16.67%	
9	0.419	0.244	2.962	3.921	0.175	52.79%	-0.959	27.87%	
10	0.243	0.776	1.224	1.848	-0.533	104.61%	-0.624	104.61%	



Table 10(on next page)

Mean unscaled displacement values in cm at points 1-10 on *Chelonia* FE models. Mean values were calculated by taking five unscaled displacement values at each location as indicated on Figures 16 and 17.



Poir	n <i>Chelonia</i>	Chelonia	Chelonia	Chelonia	Chelonia	Chelonia	Chelonia	Chelonia
t	cranium CT	cranium	mandible	mandible	cranium	cranium	mandible	mandible
	displaceme	surface scar	СТ	surface scar	model	model	displaceme	displaceme
	nt	displaceme	displaceme	displaceme	displaceme	displaceme	nt	nt
		nt	nt	nt	nt	nt	difference	difference
					difference	difference		percentage
						percentage		
1	0.0272	0.0747	0.0578	0.0497	-0.0475	93.23%	0.0081	15.07%
2	0.0244	0.0651	0.1660	0.0886	-0.0407	90.95%	0.0774	60.80%
3	0.0147	0.0390	0.1840	0.1660	-0.0243	90.50%	0.0180	10.29%
4	0.0128	0.0264	0.1450	0.1020	-0.0136	69.39%	0.0430	34.82%
5	0.0214	0.0537	0.1170	0.0579	-0.0323	86.02%	0.0591	67.58%
6	0.0237	0.0622	0.1350	0.0622	-0.0385	89.64%	0.7728	73.83%
7	0.0268	0.0731	0.1540	0.0703	-0.0463	92.69%	0.0837	74.63%
8	0.0123	0.0247	0.1740	0.1320	-0.0124	67.03%	0.0420	27.45%
9	0.0184	0.0449	0.1690	0.1270	-0.0265	83.73%	0.0420	28.38%
10	0.0251	0.0648	0.0635	0.0547	-0.0397	88.32%	0.0088	14.89%